

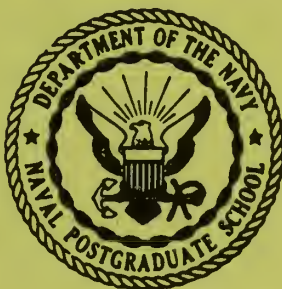
Vladislav Bevc

BEHAVIOR OF GYROTROPIC PLASMA SEPARATION  
CONSTANTS AS FUNCTIONS IN THE W-B PLANE.

TA7  
.U6  
no.47

Library  
U. S. Naval Postgraduate School  
Monterey, California

# UNITED STATES NAVAL POSTGRADUATE SCHOOL



BEHAVIOR OF GYROTROPIC PLASMA SEPARATION  
CONSTANTS AS FUNCTIONS IN THE  $\omega - \beta$  PLANE

by

Vladislav Bevc

Research Paper No. 47

February 1965

Library  
U. S. Naval Postgraduate School  
Monterey, California

BEHAVIOR OF GYROTROPIC PLASMA SEPARATION CONSTANTS  
AS FUNCTIONS IN THE  $\omega - \beta$  PLANE

by

Vladislav Bevc

U. S. Naval Postgraduate School  
Monterey, California

RESEARCH PAPER NO. 47

This work was supported in part by the Office of Naval Research

TH 7.116  
no. 47

## ACKNOWLEDGMENT

The research leave and the financial support of the Office of Naval Research as well as the use of the U. S. Naval Postgraduate School Computer Facility is gratefully acknowledged.





## BEHAVIOR OF SEPARATION CONSTANTS FOR FINITE GYROMAGNETIC PLASMAS

### Abstract

The type of the functions appearing in the expression for electromagnetic fields in finite magnetoplasmas depends only on the properties of the medium manifested in the separation constants. The  $\omega$ - $\beta$  plane of the Brillouin diagram is partitioned into a definite number of zones characterized by the type of field solutions. The general quantitative behavior of the separation constant for finite magnetoplasma in a longitudinal magnetic field on the Brillouin diagram is described.



## BEHAVIOR OF GYROTROPIC PLASMA SEPARATION CONSTANTS AS FUNCTIONS IN THE $\omega$ - $\beta$ PLANE

Of the numerous papers<sup>1</sup> concerned with the propagation of waves through waveguides filled with gyrotropic plasma columns the majority is confined either to the quasi-static approximation<sup>2,3,4,5</sup> or to a discussion of the problem in general terms with tabulation of auxiliary functions<sup>7</sup>, such as, e.g., the biradial functions<sup>8</sup> and an outline of the general method of approach for obtaining the solution<sup>6,7,9,10</sup> without a systematic and comprehensive presentation and classification of the numerous types of  $\omega$  -  $\beta$  propagation diagrams and field solutions such as are known, e.g., for empty waveguides or waveguides filled with the dielectrics<sup>11</sup> and for slow wave structures.<sup>12</sup> Only a few representative solutions have been published thus far<sup>13,14,15</sup> and they did not include a complete systematic survey of all possible cases although they were certainly oriented in this direction.

Despite a high number of combinations that can arise with the several parameters that can be varied, viz., the plasma density or the corresponding plasma frequency  $\omega_p$ , the intensity of the collimating magnetic field or the corresponding cyclotron frequency  $\omega_{cy}$ , and the diameter of the waveguide or the corresponding empty waveguide cutoff frequency, it is nevertheless possible to establish a system of classification of modes of propagation.

It is believed that one way to make it possible readily to obtain the actual solutions for given conditions in waveguides is to prepare



catalogues where quantities of interest such as, e.g., the arguments of Bessel functions, biradial functions, and the like are tabulated and presented graphically on charts and diagrams as functions in the  $\omega - \beta$  plane for various combinations of values of the plasma frequency, cyclotron frequency, and the cutoff frequency of the empty waveguide. In addition to these, actual solutions for combinations of the above values in reasonable and suitably chosen steps would also be catalogued.

The objective of this paper is to present a study of the separation constants, if indeed these quantities may be called by this name, which in circular cylindrical geometry appear as arguments of Bessel functions in the expressions for the electromagnetic fields<sup>6,7,9,10</sup>, viz.,

$$E_z = \frac{c_1 J_n(u_1 \frac{r}{a}) + c_2 J_n(u_2 \frac{r}{a})}{u_1^2 - u_2^2} \quad (1)$$

$$H_z = \frac{c_1 y(u_1) J_n(u_1 \frac{r}{a}) + c_2 y(u_2) J_n(u_2 \frac{r}{a})}{u_1^2 - u_2^2} \quad (2)$$

Evidently, the separation constants determine the kind of the Bessel functions in Eqs. 1 and 2. If either  $u_1$  or  $u_2$  or both are imaginary, the corresponding Bessel function become modified,  $I_n$  instead of  $J_n$ . If they are complex conjugates Bessel functions of complex arguments appear in the above expressions. It is therefore believed that it is more



useful to know the behavior of the separation constants  $u_1$  and  $u_2$  in the  $\omega - \beta$  plane than merely the behavior of the separate components of the equivalent dielectric tensor  $\underline{\epsilon}$  which is sometimes presented.

The constants  $u_1$  and  $u_2$  are solutions of a biquadratic equation which is obtained solely from the properties of the medium. In addition, of course, they must like,  $c_1$  and  $c_2$ , also be compatible with the boundary conditions. The medium or electronic equation was first derived by Hahn<sup>6</sup> and we shall give it in its original form:

$$\left[ \left( \frac{u}{a} \right)^2 + \beta^2 + k_p^2 - k^2 \right]^2 = \frac{k_{cy}^2}{(k^2 - k_p^2)} \left[ \left( \frac{u}{a} \right)^2 + \beta^2 - k^2 \right] \left[ \left( \frac{u}{a} \right)^2 + \left( 1 - \frac{k_p^2}{k^2} \right) (\beta^2 - k^2) \right] \quad (3)$$

The following notation is being used here:

$$k_p = \frac{\omega_p}{c} \quad (4-a)$$

$$\omega_p = \sqrt{\frac{e\rho_0}{m\epsilon_0}} \quad (4-b)$$

$$k_{cy} = \frac{\omega_{cy}}{c} \quad (4-c)$$

$$\omega_{cy} = \mu_0 \frac{e}{m} H_0 \quad (4-d)$$

$$k = \frac{\omega}{c} \quad (4-e)$$







Symbols denoting the quantities are as follows:

$\omega$  = frequency at which the waves in waveguide propagate;

$\rho_0$  = electronic volume charge density;

$\beta$  = propagation constant appearing in the expression  $\exp j(\omega t - \beta z)$ ;

$c$  = velocity of light;

$e/m$  =  $1.76 \times 10^{11}$  coulomb/Kg, electron charge to mass ratio;

$H_0$  = axial static magnetic field strength;

$\mu_0$  =  $1.25 \times 10^{-6}$  henry/m;

$E_0$  =  $8.86 \times 10^{-12}$  farad/m;

$a$  = radius of the cylindrical waveguide.

The explicit solution of the biquadratic equation is:

$$\left(\frac{u_{1,2}}{a}\right)^2 = \frac{1}{2(k^2 - k_p^2 - k_{cy}^2)} \left\{ - \left[ 2(k^2 - k_p^2 - k_{cy}^2) + \frac{k_p^2 k_c^2}{k^2} \right] (\beta^2 - k^2) - 2(k^2 - k_p^2) k_p^2 \right. \\ \left. \pm \frac{k_{cy}^2 k_p^2}{k^2} \sqrt{(\beta^2 - k^2)^2 + 4\beta^2 \frac{k^2}{k_{cy}^2} (k^2 - k_p^2)} \right\} \quad (5)$$

The plus sign in front of the square root will be consistently used for the calculation of  $u_1^2$  and the negative sign for the calculation of  $u_2^2$ .

It is evident that we may multiply the Equation (5) by  $a^2$  throughout and then obtain  $u^2$  expressed in terms of  $ka$ ,  $k_p a$ ,  $k_{cy} a$ ,  $\beta a$  which is useful for representation on diagrams since these values are then pure



numbers.

The following relationship holds between the function  $u^2$  and the function  $\chi^2$  used by Suhl and Walker<sup>10</sup>:

$$\chi_{1,2}^2 = \frac{u_{1,2}^2}{(ka)^2 - (k_p a)^2} \quad (6)$$

It appears that the reason for the use of this expression by Suhl and Walker was the desire for unified treatment of both ferrite and plasma filled waveguides. Apparently propagation was not expected for values of frequency lower than the value of plasma frequency. A numerical solution of the equations of Suhl and Walker would have discovered the plasmaguide modes that were later found by Trivelpiece and Gould<sup>2</sup>.

Camus and Le Mezec<sup>14</sup> use the notation:

$$T^2 = \frac{u^2}{a^2} \quad (7)$$

and

$$Z = \frac{u^2}{(k_p a)^2} \quad (8)$$

When boundary conditions are introduced it is best to normalize all frequencies to the frequency defined by:

$$\omega_0 = c/a \quad (9)$$



This means that quantities  $k_p a$ ,  $k_{cy}$ ,  $ka$  can be considered essentially as  $\omega_p$ ,  $\omega_{cy}$ ,  $\omega$  normalized with respect to  $\omega_0$ . Whenever boundary conditions are introduced the radius of the waveguide appears in the expression and both plasma frequency  $\omega_p$  and cyclotron frequency  $\omega_{cy}$  are specified by  $k_p a$  and  $k_{cy} a$  respectively, i.e., in terms of the normalizing frequency  $\omega_0 = c/a$ . The solution of the boundary condition problem depends on the absolute value of  $\omega_p$  and  $\omega_{cy}$ . However, when we consider only the quantities  $u_1^2$  and  $u_2^2$  as functions of the frequency  $\omega$  and wave number  $\beta$ , i.e., as functions in the  $\omega - \beta$  plane it is possible to normalize all frequencies to the plasma frequency (or alternatively to the cyclotron frequency) and the ratio of the cyclotron frequency to the plasma frequency becomes the only parameter that is left to be varied. This ratio is denoted in the following way:

$$M = \frac{\omega_{cy}}{\omega_p} = \frac{(k_{cy} a)}{(k_p a)} \quad (10)$$

Likewise, it is convenient to normalize the other quantities with respect to the plasma frequency:

$$Y = \frac{(ka)}{(k_p a)} = \frac{\omega}{\omega_p} \quad (11)$$

$$X = \frac{\beta a}{(k_p a)} = \frac{\beta c}{\omega_p} \quad (12)$$



In this normalization the Hahn's equation for  $u_1^2$  and  $u_2^2$  reads:

$$U_{1,2}^2 = \frac{u_{1,2}^2}{(k_p a)^2} = \frac{1}{2(Y^2 - 1 - M^2)} \left\{ - \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right] (X^2 - Y^2) - 2(Y^2 - 1) \right. \\ \left. \pm \frac{M^2}{Y^2} \sqrt{(X^2 - Y^2)^2 + \frac{4X^2 Y^2}{M^2} (Y^2 - 1)} \right\} \quad (13)$$

Note that  $U_1^2$  and  $U_2^2$  are multivalued at the origin ( $X=0, Y=0$ ). Its value depends on the path in the  $Y$ - $X$  plane along which we approach the origin. It is seen without difficulty that the values of  $U_{1,2}^2$  are real for values of  $X$  and  $Y$  exterior to the region in which the expression under the square root becomes negative, viz.,

$$0 < Y < 1 \quad (14)$$

$$\frac{Y}{M} \left[ \sqrt{1 + M^2 - Y^2} - \sqrt{1 - Y^2} \right] < X < \frac{Y}{M} \left[ \sqrt{1 + M^2 - Y^2} + \sqrt{1 - Y^2} \right] \quad (15)$$

Within this region the values of  $U_1^2$  and  $U_2^2$  are complex conjugates.

The boundary of the complex region is a closed curve touching the line

$$Y = 1 \text{ at } X = 1 \text{ and the line } X = \sqrt{\frac{1 + M^2}{M^2}} \text{ at } Y = \sqrt{\frac{1 + M^2}{2 + M^2}}. \text{ As } M \text{ is}$$

increased the complex region becomes narrower. This boundary is also

shown on Figures 1 to 4 and 6 to 15. On the above boundary curve







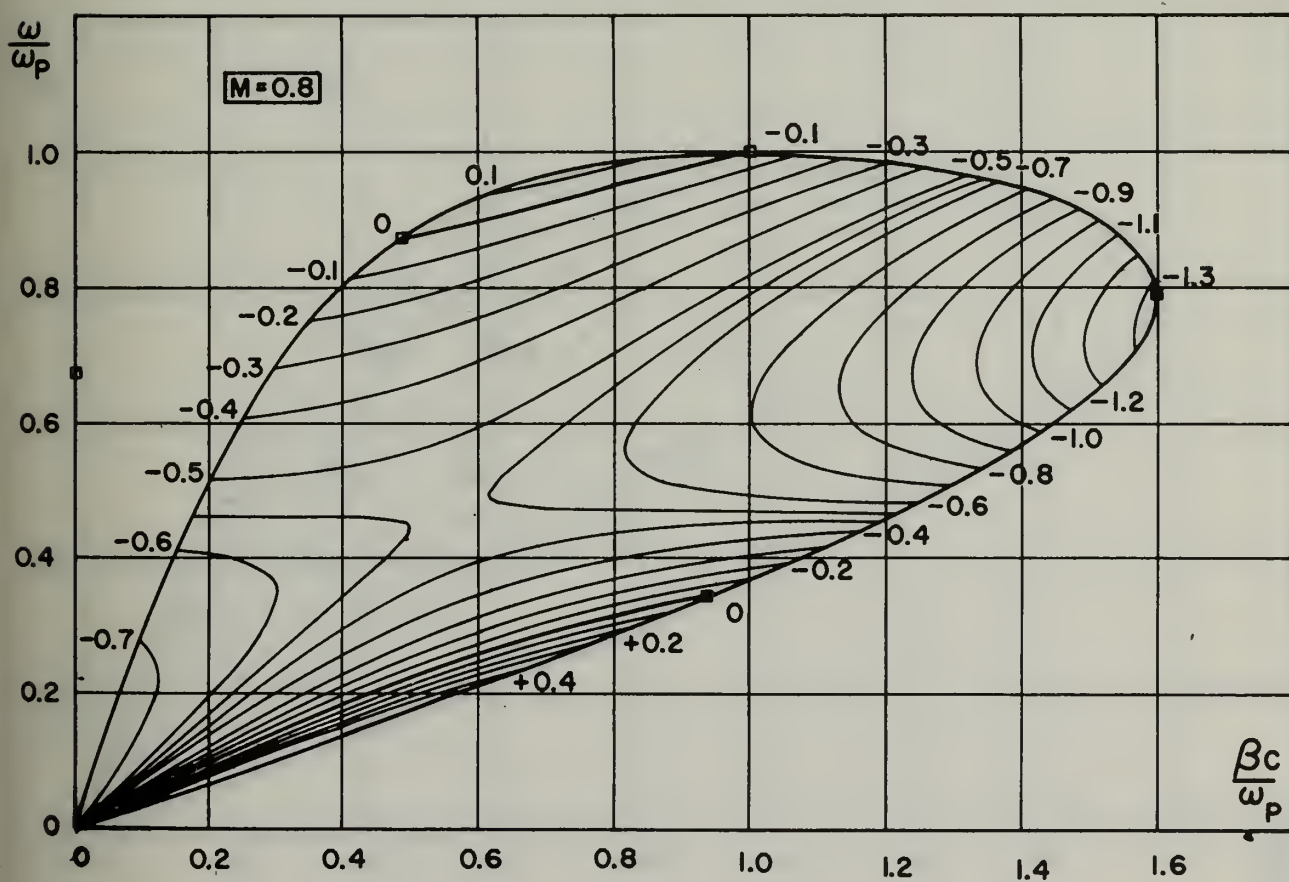


Fig. 1 Contour curves for constant values of  $\text{Re}(U^2)$  in the complex region of the  $\omega = \beta$  plane at the value of  $M = 0.8$ .



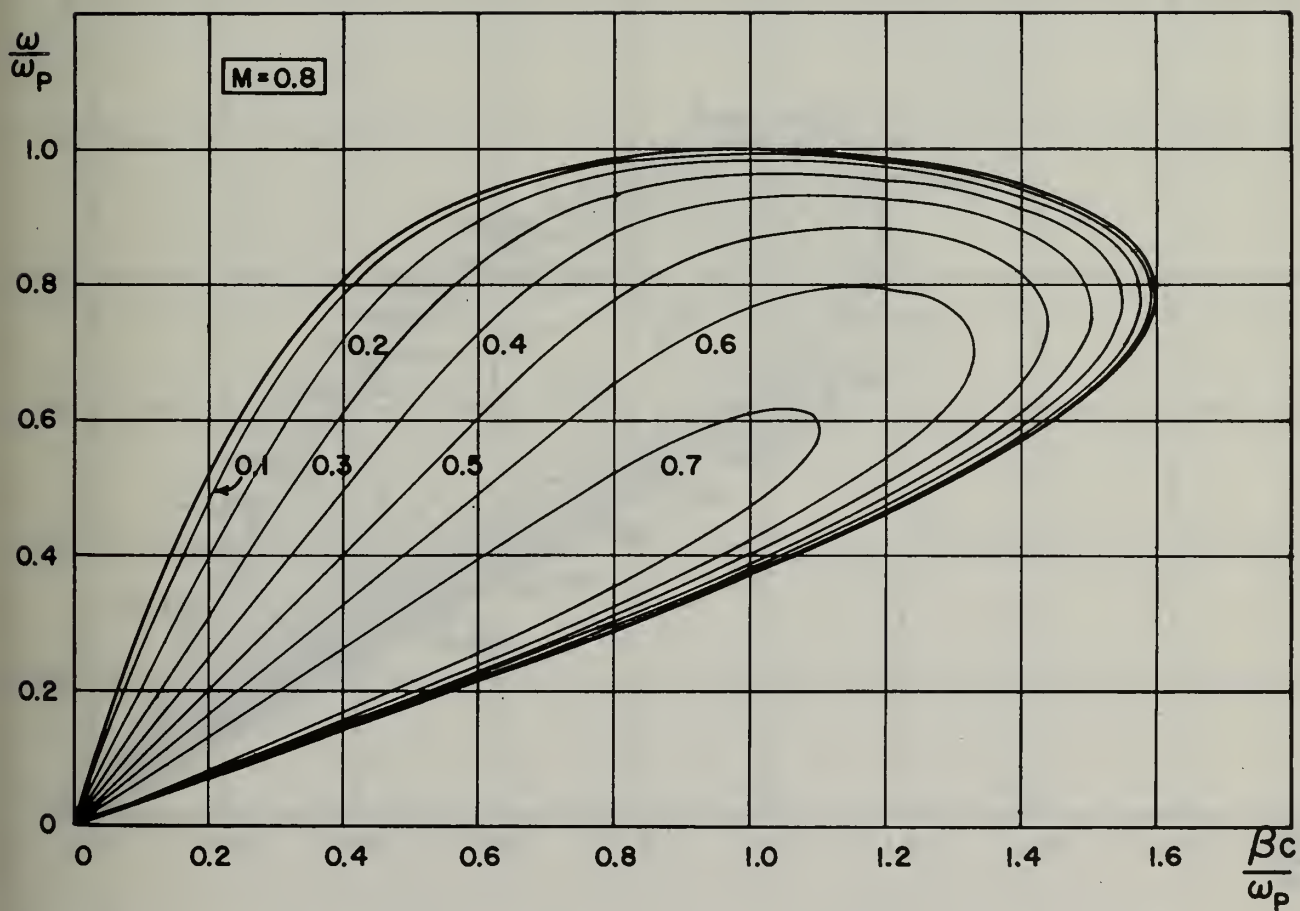


Fig. 2 Contour curves for constant values of  $\text{Im}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .



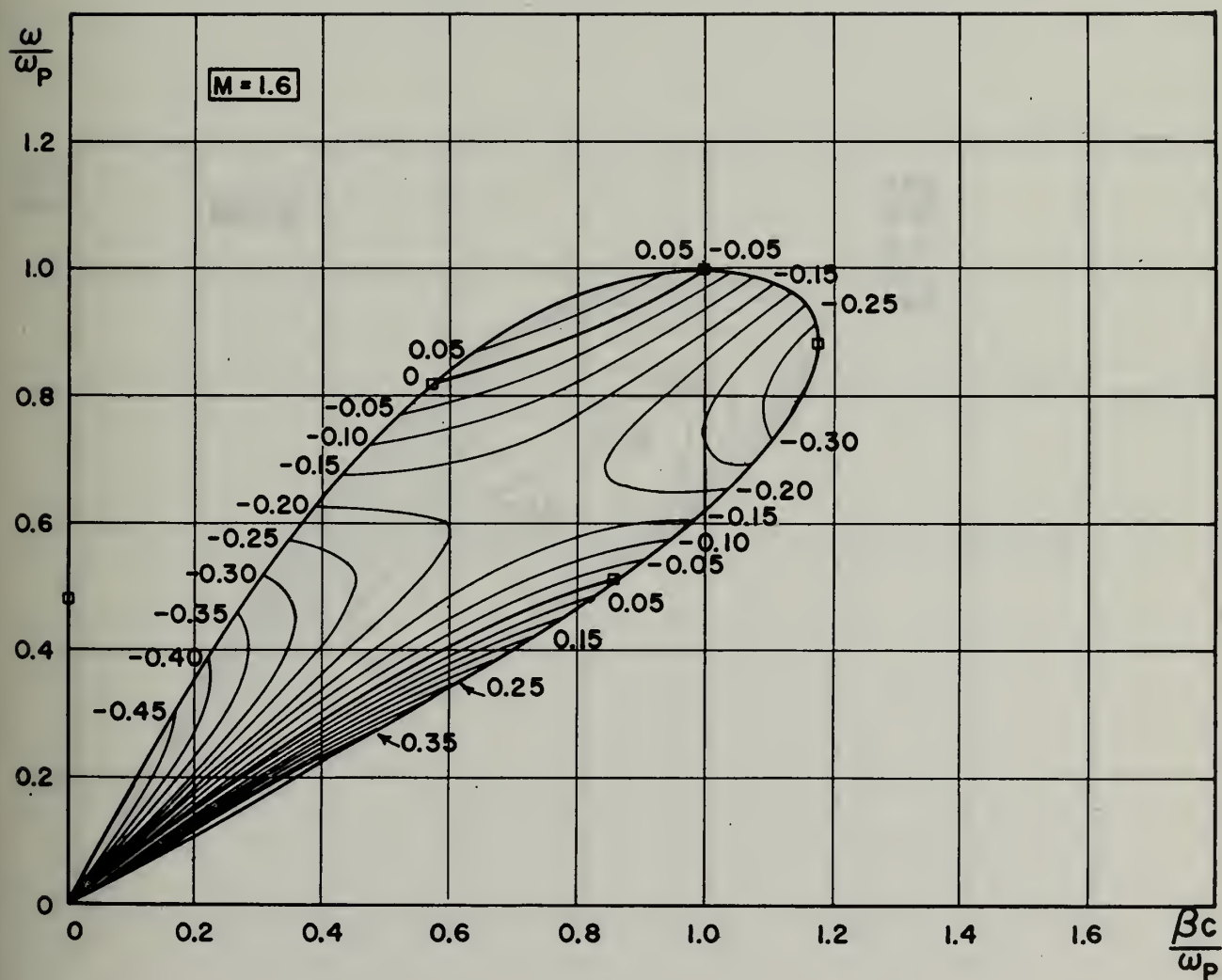


Fig. 3 Contour curves for constant values of  $\text{Re}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .



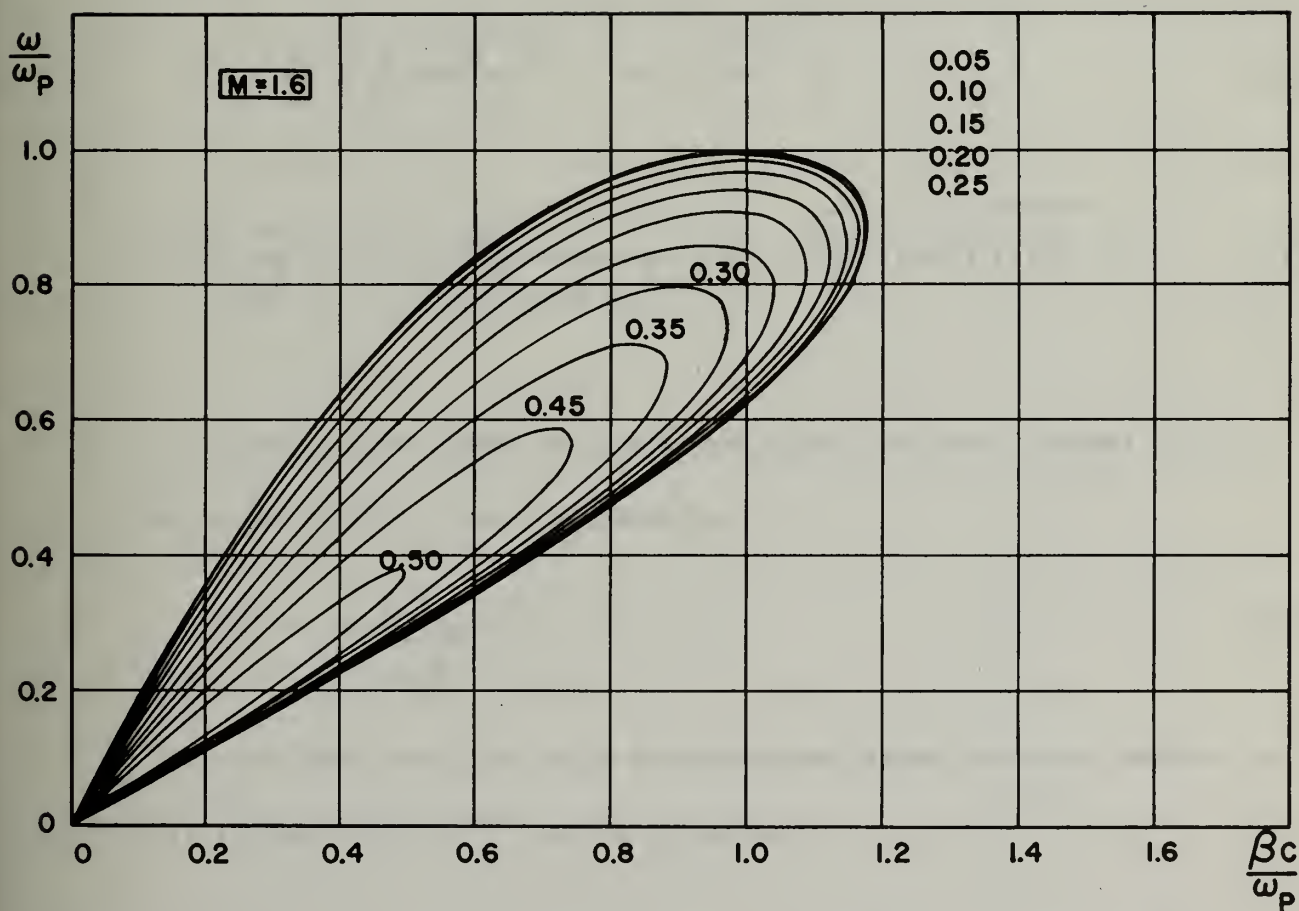


Fig. 4 Contour curves for constant values of  $\text{Im}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .







(Eqs. 14 and 15) the expression under the square root vanishes and  $U_1^2 = U_2^2$ . The values of  $U_1^2 = U_2^2$  on the boundary curve are:

$$\text{on } X = \frac{Y}{M} \left[ \sqrt{1 + M^2 - Y^2} - \sqrt{1 - Y^2} \right] \quad (16)$$

$$U^2 = 2 \frac{Y^2}{M^2} \left\{ Y^2 - 1 - \left[ \frac{M^2}{2Y^2(1 + M^2 - Y^2)} - 1 \right] \sqrt{(M^2 + 1 - Y^2)(1 - Y^2)} \right\} \quad (17)$$

and on

$$X = \frac{Y}{M} \left[ \sqrt{1 + M^2 - Y^2} + \sqrt{1 - Y^2} \right] \quad (18)$$

$$U^2 = 2 \frac{Y^2}{M^2} \left\{ Y^2 - 1 + \left[ \frac{M^2}{2Y^2(1 + M^2 - Y^2)} - 1 \right] \sqrt{(M^2 + 1 - Y^2)(1 - Y^2)} \right\} \quad (19)$$

If the origin ( $X=0, Y=0$ ) is approached along the curve defined in Eq. 16 the value of  $U^2$  at zero is given by

$$U^2 = - \frac{1}{\sqrt{1 + M^2}} \quad (20)$$

if on the other hand the origin is approached along the curve defined in Eq. 18 the value of  $U^2$  at zero is given by

$$U^2 = + \frac{1}{\sqrt{1 + M^2}} \quad (21)$$



The equations of contour lines  $\text{Re}(U^2) = \text{const}$  and  $\text{Im}(U^2) = \text{const}$  within the region defined by Eq. 14 and 15 are readily found. For  $\text{Re}(U^2) = \text{constant}$

$$X = \sqrt{Y^2 + 2 \frac{(1-Y^2) + (1+M^2-Y^2)\text{Re}(U^2)}{\left[ \frac{M^2}{Y^2} - 2(M^2+1-Y^2) \right]}} \quad (22)$$

for  $\text{Im}(U^2) = \text{constant}$

$$X = \frac{Y}{M} \sqrt{(M^2+1-Y^2) + (1-Y^2) \pm 2 \sqrt{(1-Y^2)(1+M^2-Y^2) - (M^2+1-Y^2)^2 (\text{Im}(U^2))^2}} \quad (23)$$

The curves given by Eq. 22 are single valued functions of  $Y$  while the curves given by Eq. 23 are double valued; they are closed curves similar to the boundary of the region. Figures 1 to 4 show representative contour diagrams inside the complex region. It is further of interest to determine whether and in which points on the boundary curve the value of  $U^2$  vanishes. Evidently  $U^2=0$  at  $Y=1$  and  $X=1$ , other points are found by setting the expressions of Eq. 17 or 19 equal to zero, and arrange the terms in powers of  $Y^2$ . Thus we obtain:

$$Y^6 - (2+M^2)Y^4 + (1+M^2)Y^2 - \frac{M}{4} = 0 \quad (24)$$

The roots of this equation are real as would become apparent if Eq. 24 were solved; it is possible to obtain them by solving them numerically. However,



a more elegant way to study its roots is available. It will be recalled that either  $U_1^2$  or  $U_2^2$  can vanish on the following two curves:

$$X = \sqrt{Y^2 - \frac{1}{1 - \frac{M}{Y}}} \quad (25)$$

$$X = \sqrt{Y^2 - \frac{1}{1 + \frac{M}{Y}}} \quad (26)$$

These two curves lie outside of the complex region. Equation 25 represents a curve with a discontinuity at  $Y = M$ , its upper branch intercepts the  $Y$  axis (corresponding to  $\omega$  axis) at  $Y = + \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1}$ ;

Eq. 26 represents a continuous curve with  $Y$  intercept at

$Y = - \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1}$ . Values of  $U_1^2$  and  $U_2^2$  on curves given by Equations 25 and 26 can be readily evaluated. On the curve given by

Eq. 25 we have:

$$U_{1,2}^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left[ \frac{Y^3 - MY^2 - Y + M/2}{Y - M} \pm \sqrt{\left( \frac{Y^3 - MY^2 - Y + M/2}{Y - M} \right)^2} \right] \quad (27)$$

Care must be exercised in taking the square root in this expression.

We shall here take the square root as the opposite operation of squaring.

The expression under the square root is always positive but the expression squared can be either positive or negative. For the sign of the square root we take the sign of the squared quantity which we must first evaluate.



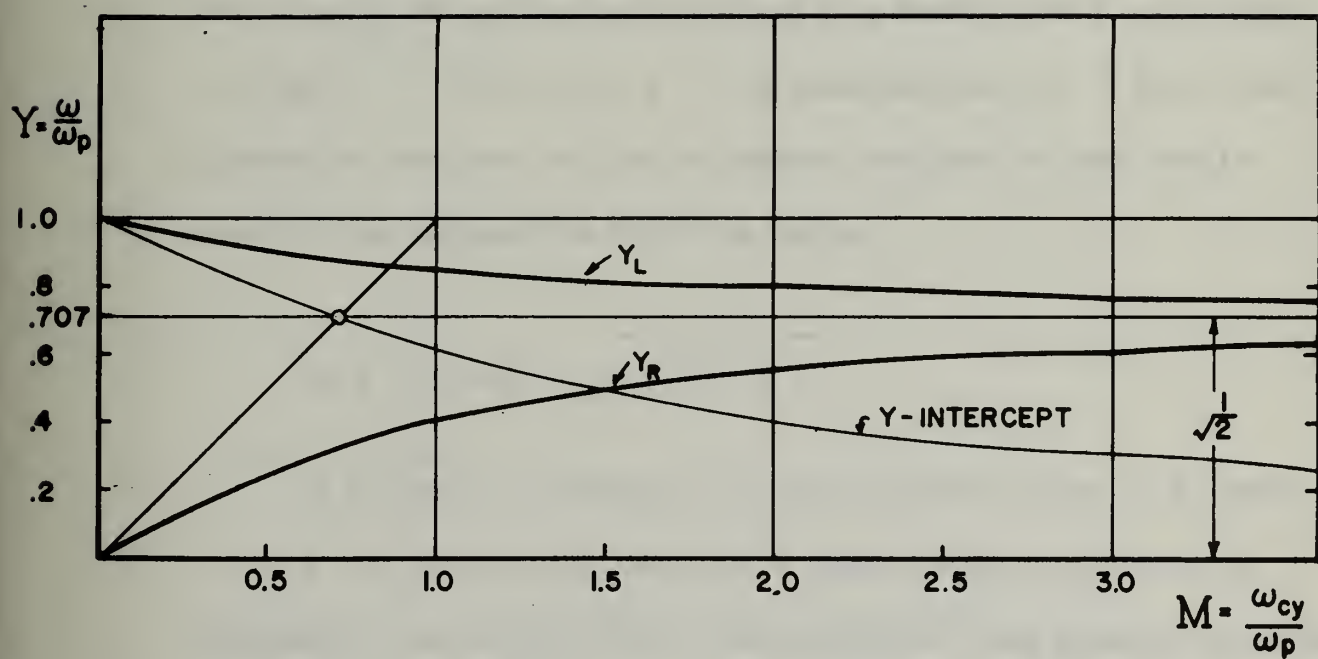


Fig. 5 Plot of the parameter  $M$  as a function of  $Y(=\omega/\omega_p)$  illustrating the solutions of the cubic of Eq. 28.





The roots of the cubic equation

$$Y^3 - MY^2 - Y + \frac{M}{2} = 0 \quad (28)$$

may be determined as follows. From Eq. 28 we have

$$M = \frac{Y(Y-1)(Y+1)}{(Y - \frac{1}{\sqrt{2}})(Y + \frac{1}{\sqrt{2}})} \quad (29)$$

The value of  $M$  can be readily plotted as a function of  $Y$  as is shown on Fig. 5. From Fig. 5 it is seen that one root of Eq. 28 designated as first root, is always negative and that the third root is always found between the following limits:

$$M < Y_3 < \frac{M}{2} + \sqrt{\left(\frac{M}{2}\right)^2 + 1} \quad (30)$$

If we limit our interest to the first quadrant of the  $\omega$ - $\beta$  plane ( $Y > 0, X > 0$ ) and to real values of  $X$  these two roots need not be considered. The second root, on the other hand, lies between the values

$$0 < Y_2 < \frac{1}{\sqrt{2}} \quad (31)$$

This means that a point exists on the lower branch of the curve given by Eq. 25 with an ordinate  $Y$  which satisfies the cubic of Eq. 28 and as a consequence both  $U_1^2$  and  $U_2^2$  are equal to zero in that point. If both



$U_1^2$  and  $U_2^2$  are equal to zero then they are also equal to each other and consequently lie on the curve given by Eq. 18, i.e., on the right boundary of the region of complex values of  $U_1^2$  and  $U_2^2$ . Hence the curve of Eq. 25 has one point in common with the right boundary of the complex region given by Eq. 18 and the two curves are tangent to each other in that point. We shall call this point the lower tangent point. Now for values of  $Y$  between zero and the second root  $Y_2$  of Eq. 28 the squared expression in Eq. 27 is negative, viz.,

$$Y^3 - MY^2 - Y + \frac{M}{2} > 0 \quad (32)$$

$$Y - M < 0 \quad (33)$$

$$\text{if } 0 < Y < Y_2 \quad (34)$$

From where follows for  $U_1^2$

$$U_1^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left\{ \frac{Y^3 - MY - Y + M/2}{Y - M} + \left( -\frac{Y^3 - MY - Y + M/2}{Y - M} \right) \right\} = 0 \quad (35)$$

and for  $U_2^2$ :

$$U_2^2 = \frac{2M(Y^3 - MY - Y + M/2)}{Y(Y^2 - 1 - M^2)(Y - M)} \quad (36)$$



When, on the other hand, the value of  $Y$  is greater than the value of the second root the following relations hold:

$$Y^3 - MY^2 - Y + \frac{M}{2} < 0 \quad (37)$$

$$Y - M < 0 \quad (38)$$

$$Y_2 < Y < M \quad (39)$$

The squared quantity in Eq. 27 is then positive and we have

$$U_1^2 = \frac{2M(Y^3 - MY^2 - Y + M/2)}{Y(Y^2 - 1 - M^2)(Y - M)} \quad (40)$$

$$U_2^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left\{ \frac{Y^3 - MY^2 - Y + M/2}{Y - M} - \frac{Y^3 - MY^2 - Y + M/2}{Y - M} \right\} = 0 \quad (41)$$

Thus it is seen that on the curve given by Eq. 35 between the origin ( $X=0$ ,  $Y=0$ ) and the point in which this curve touches the boundary of the complex region the function  $U_1^2$  is zero and the function  $U_2^2$  has a value given by Eq. 40, on the rest of the curve, beyond the lower tangent point, the situation is reversed and the function  $U_2^2$  is zero while the function  $U_1^2$  is given by Eq. 40. Likewise it can be seen that on the upper branch of the curve given by Eq. 25 the value of the function  $U_2^2$  is always zero and the value of the function  $U_1^2$  is given by Eq. 40 for positive values



of  $Y$ .

In the same manner we obtain the values of  $U_1^2$  and  $U_2^2$  on the curve given by Eq. 26.

$$U_{1,2}^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left\{ -\frac{Y^3 + MY^2 - Y - M/2}{Y + M} \pm \sqrt{\left(\frac{Y^3 + MY^2 - Y - M/2}{Y + M}\right)^2} \right\} \quad (42)$$

To determine the sign of the square root it is again necessary to study the behavior of the cubic polynomial and the roots of the equation

$$Y^3 + MY^2 - Y - \frac{M}{2} = 0 \quad (43)$$

It is immediately obvious that this equation becomes identical to Eq. 28 if the variable  $Y$  is replaced by  $-Y$ . The roots are then as shown on Fig. 5 only with the positive and negative  $Y$  axis interchanged. From the same considerations as before only the positive root, designated henceforth as the third root (of Eq. 43) is of interest. The third root lies between the values

$$\frac{1}{\sqrt{2}} < Y_3 < 1 \quad (44)$$

This again, means that a point exists on the curve given by Eq. 26 with an ordiante  $Y_3$  which satisfies the cubic of Eq. 43 and consequently both  $U_1^2$  and  $U_2^2$  are equal to zero in that point and, according to the argument







presented before, this point, too, lies on the curve given by Eq. 16, i.e., on the left boundary of the region of complex values of  $U_1^2$  and  $U_2^2$ . Thus the curve of Eq. 26 has a point in common with the left boundary of the complex region given by Eq. 16, the two curves are tangent to each other at that point. We shall call this point the upper tangent point. Now for values of  $Y$  between the ordinate intercept of the curve given by the Eq. 26 and the third root, viz.,

$$-\frac{M}{2} + \sqrt{\left(\frac{M}{2}\right)^2 + 1} < Y < Y_3 \quad (45)$$

the squared expression in Eq. 42 is negative

$$Y^3 + MY^2 - Y - \frac{M}{2} < 0 \quad (46)$$

From where follows for  $U_1^2$

$$U_1^2 = \frac{-2M}{Y(Y^2 - 1 - M^2)} \left[ \frac{Y^3 + MY^2 - Y - M/2}{Y + M} \right] \quad (47)$$

and for  $U_2^2$

$$U_2^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left[ -\frac{Y^3 + MY^2 - Y - M/2}{Y + M} - \left( -\frac{Y^3 + MY^2 - Y - M/2}{Y + M} \right) \right] = 0 \quad (48)$$



when, on the other hand, the value of  $Y$  is greater than the value of the third root the following relations hold

$$Y^3 + MY^2 - Y - \frac{M}{2} > 0 \quad (49)$$

$$Y > Y_3 \quad (50)$$

The squared quantity in Eq. 42 is then positive and we have for  $U_1^2$

$$U_1^2 = \frac{M}{Y(Y^2 - 1 - M^2)} \left[ -\frac{Y^3 + MY^2 - Y - M/2}{Y+M} + \left( \frac{Y^3 + MY^2 - Y - M/2}{Y+M} \right) \right] = 0 \quad (51)$$

and for  $U_2^2$

$$U_2^2 = \frac{-2M}{Y(Y^2 - 1 - M^2)} \left[ \frac{Y^3 + MY^2 - Y - M/2}{Y+M} \right] \quad (52)$$

In the same manner it can be shown that on the left boundary of the complex region given by Eq. 16 the values of  $U^2$  are negative for values of  $Y$  smaller than the value of the third root ( $Y < Y_3$ ) and positive for values of  $Y$  greater than the value of the third root ( $Y_3 < Y < 1$ ) and that on the right boundary given by Eq. 18 the values of  $U^2$  are positive for values of  $Y$  smaller than the value of the second root ( $Y < Y_2$ ) and positive the values of  $Y$  greater than the value of the second root



( $Y_2 < Y < 1$ ). Moreover it can be seen that on the line  $Y=1$  the values of functions  $U_1^2$  and  $U_2^2$  are as follows:

In the interval:

$$Y=1, 0 < X < 1 \quad (53)$$

$$U_1^2 = 0 \quad (54)$$

$$U_2^2 = 1 - X^2 \quad (55)$$

and in the interval:

$$Y=1, 1 < X < \infty \quad (56)$$

$$U_1^2 = 1 - X^2 \quad (57)$$

$$U_2^2 = 0 \quad (58)$$

To show that the roots of Equations 28 and 43 are also the roots of Eq. 24 obtained for the condition that both  $U_1^2$  and  $U_2^2$  vanish we multiply the cubic polynomials of Equations 28 and 43; the resulting bicubic polynomial is just that of Eq. 24.

Since in the complex region the functions  $U_1^2$  and  $U_2^2$  are complex conjugates they can be represented by their modulus  $\rho$  and argument  $\varphi$ , viz.:  $U_1 = \rho \angle \varphi$ ;  $U_2 = \rho \angle -\varphi$ . Note that we have here  $U_1$  and  $U_2$  instead of  $U_1^2$  and  $U_2^2$ . Contour curves of constant



modulus and argument of the functions  $U_1$  and  $U_2$  are of greater practical value than the contour curves for constant real and imaginary part of  $U^2$ . Tables of Bessel functions of complex arguments<sup>16</sup> give the argument of the Bessel functions in polar form.

The modulus  $\rho$  is readily found from Eq. 13:

$$\rho^4 = \frac{1}{4(Y^2-1-M^2)^2} \left\{ \left[ (2(Y^2-1-M^2) + \frac{M^2}{Y^2})(X^2-Y^2) + 2(Y^2-1) \right]^2 \right. \\ \left. + \frac{M^4}{Y^4} \left[ 4 \frac{X^2 Y^2}{M^2} (1-Y^2) - (X^2-Y^2)^2 \right] \right\} \quad (59)$$

To find the equation of a contour curve in the  $Y$ - $X$  ( $\omega - \beta$ ) plane for constant value of  $\rho$  the above equation is expanded in powers of  $X^2$  and a quadratic equation in  $X^2$  is obtained.

$$C_4 X^4 + C_2 X^2 + C_0 - \rho^4 = 0 \quad (60)$$

The coefficients  $C_0, C_2, C_4$  depend only on  $Y$  and  $M$  and are given





by the expressions:

$$C_0 = \frac{\left[2(Y^2-1-M^2) + \frac{M^2}{Y^2}\right]^2 Y^4 - 4Y^2(Y^2-1) \left[2(Y^2-1-M^2) + \frac{M^2}{Y^2}\right] + 4(1-Y^2)^2 - M^4}{4(Y^2-1-M^2)^2} \quad (61)$$

$$C_2 = \frac{-2Y^2 \left[2(Y^2-1-M^2) + \frac{M^2}{Y^2}\right]^2 + 4(Y^2-1) \left[2(Y^2-1-M^2) + \frac{M^2}{Y^2}\right] + 4 \frac{M^2}{Y^2} (1-Y^2) + 2 \frac{M^4}{Y^2}}{4(Y^2-1-M^2)^2} \quad (62)$$

$$C_4 = \frac{Y^2-1-M^2 + M^2/Y^2}{Y^2-1-M^2} \quad (63)$$

From Eq. 60 we obtain the explicit form of the equation for the contour curve of constant modulus  $\rho$ .

$$X = \sqrt{-\frac{C_2}{2C_4} \pm \sqrt{\left(\frac{C_2}{2C_4}\right)^2 + \frac{\rho^4 - C_0}{C_4}}} \quad (64)$$

Obviously  $X$  must be real and positive. Some representative contour curves given by the above equation are shown on Figures 6 and 8.

The argument  $\varphi$  is also found from Eq. 13:

$$\tan(2\varphi) = \frac{\frac{M^2}{Y^2} \sqrt{4 \frac{X^2 Y^2}{M^2} (1-Y^2) - (X^2 - Y^2)^2}}{-\left[2(Y^2-1-M^2) + \frac{M^2}{Y^2}\right] - 2(Y^2-1)} \quad (65)$$

To find the equation of a contour curve for constant argument in the  $Y$ - $X$



( $\omega - \beta$ ) plane we use the notation  $T = \tan(2\varphi)$  and expand the Eq. 65 in powers of  $X^2$  so that a quadratic equation in  $X^2$  is obtained.

$$C_4' X^4 + C_2' X^2 + C_0' = 0 \quad (66)$$

The coefficients  $C_0'$ ,  $C_2'$ ,  $C_4'$  depend only on  $Y$ ,  $M$ , and  $T$  and are given by the following expressions:

$$C_0' = T^2 Y^4 \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right]^2 - 4T^2 (Y^2 - 1) Y^2 \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right] + 4T^2 (Y^2 - 1)^2 + M^4 \quad (67)$$

$$C_2' = -2Y^2 T^2 \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right]^2 + 4T^2 (Y^2 - 1) \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right] - \frac{4M^2}{Y^2} (1 - Y^2) \quad (68)$$

$$C_4' = T^2 \left[ 2(Y^2 - 1 - M^2) + \frac{M^2}{Y^2} \right]^2 + \frac{M^4}{Y^4} \quad (69)$$

From Eq. 66 we obtain the explicit form of the equation for the contour curve for constant argument.

$$X = \sqrt{-\frac{C_2'}{2C_4'}} \pm \sqrt{\left(\frac{C_2'}{2C_4'}\right)^2 - \frac{C_0'}{C_4'}} \quad (70)$$

Again,  $X$  must be real and positive. Some representative contour curves given by the above equation are shown on Figures 7 and 9.



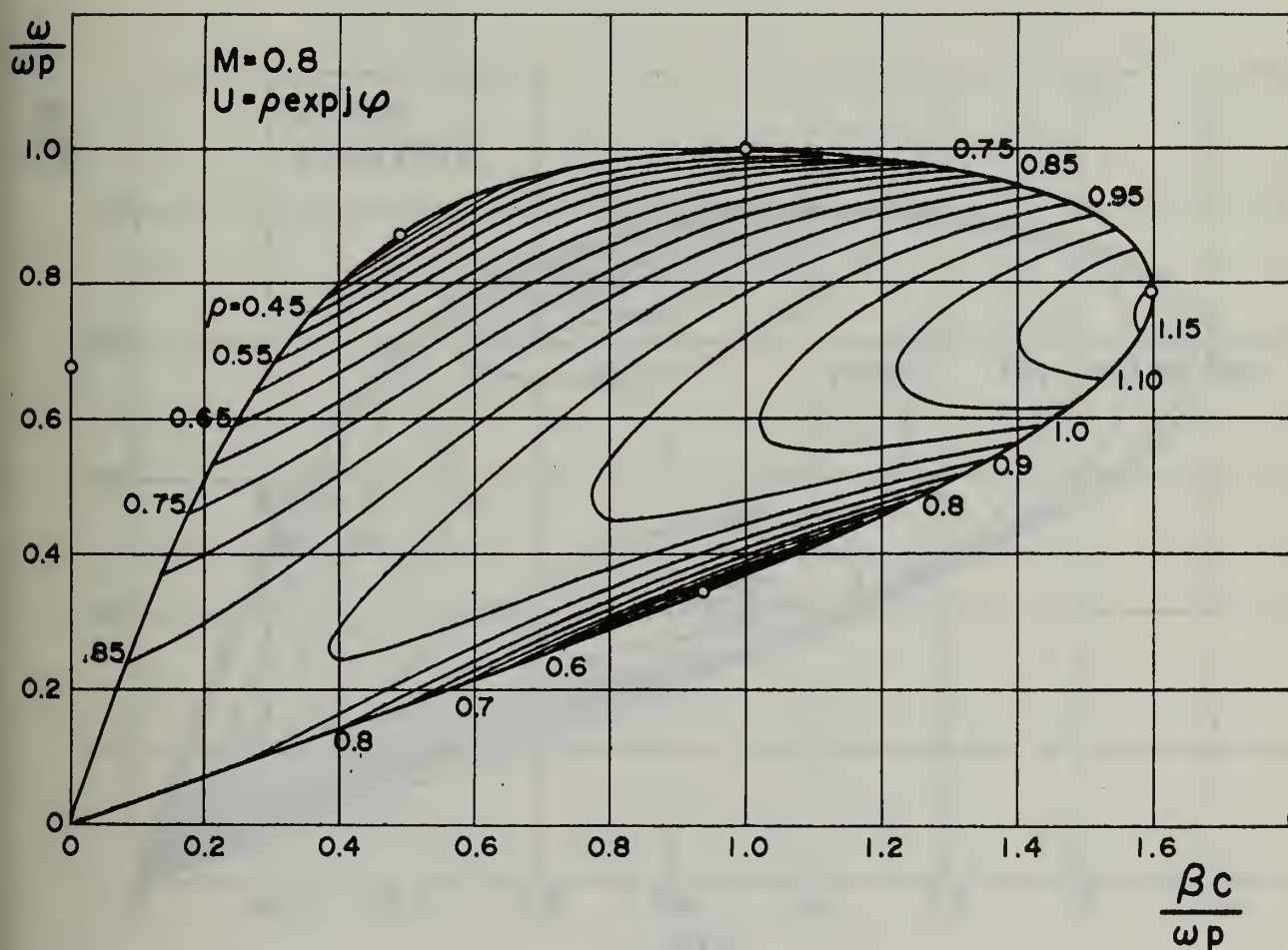


Fig. 6 Contour curves for constant values of the modulus  $\rho$  of the function  $U = \rho \exp j\varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .



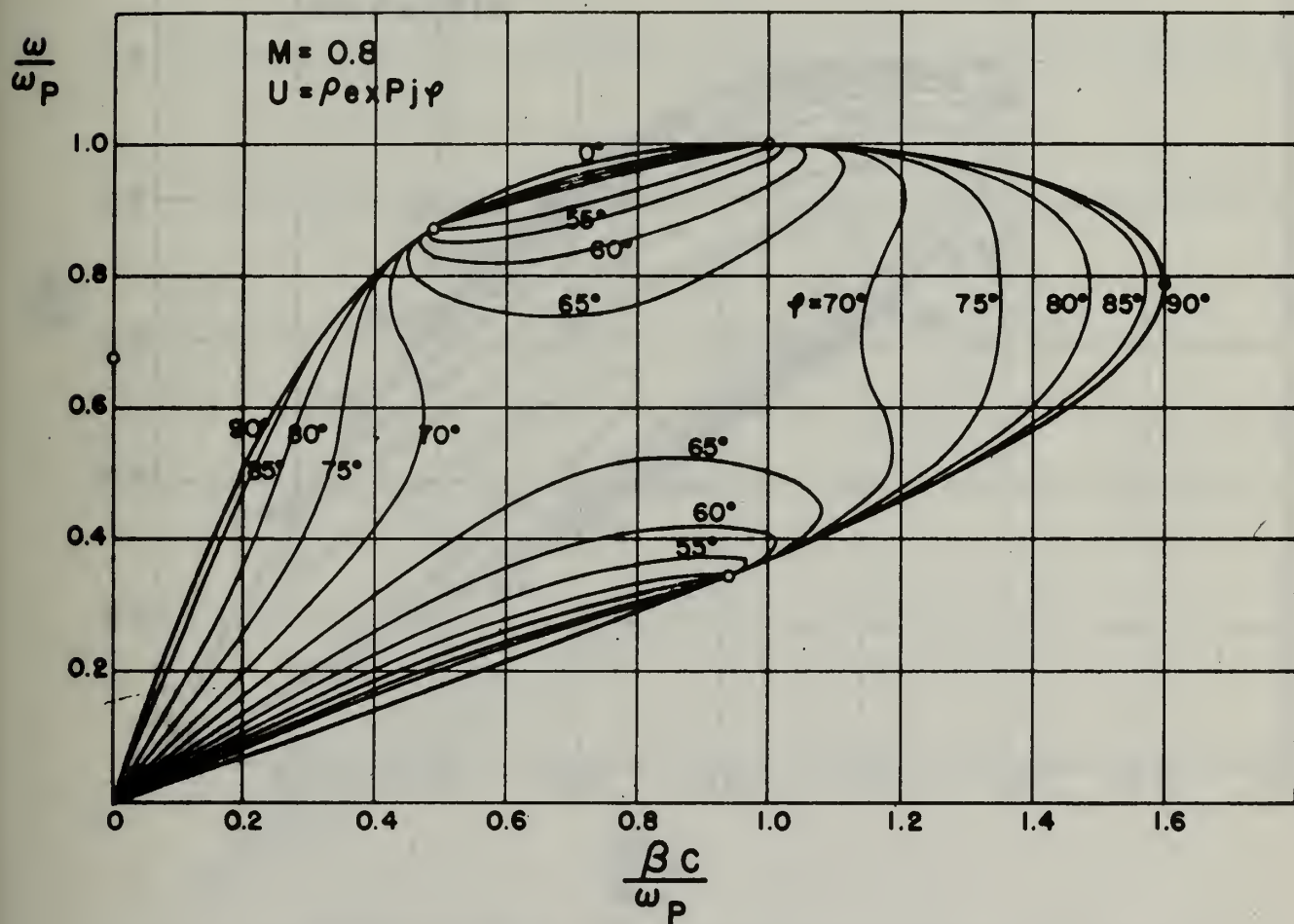


Fig. 7 Contour curves for constant values of the argument  $\varphi$  of the function  $U = \rho \exp(j\varphi)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .







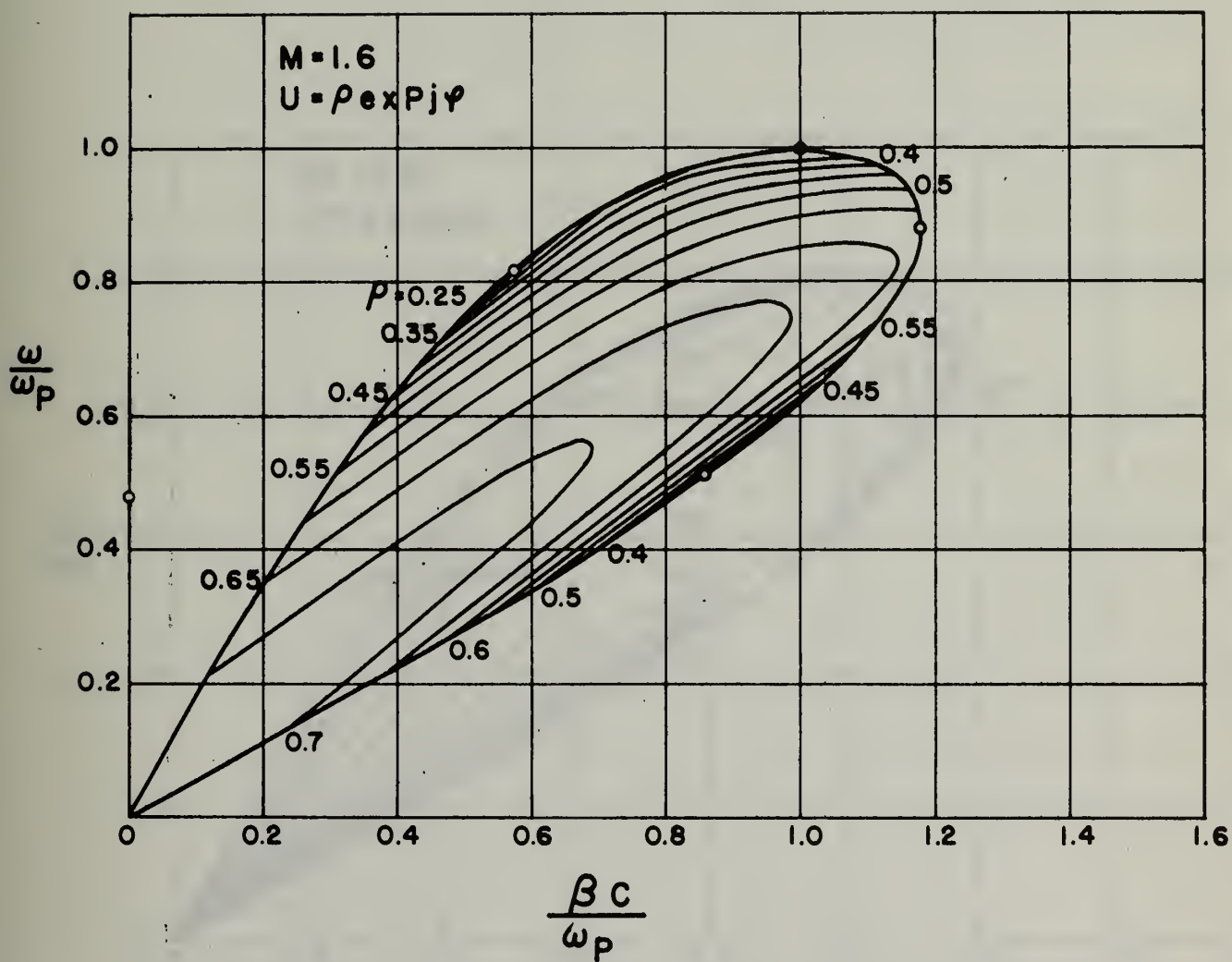


Fig. 8 Contour curves for constant values of the modulus  $\rho$  of the function  $U = \rho \exp j\varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .



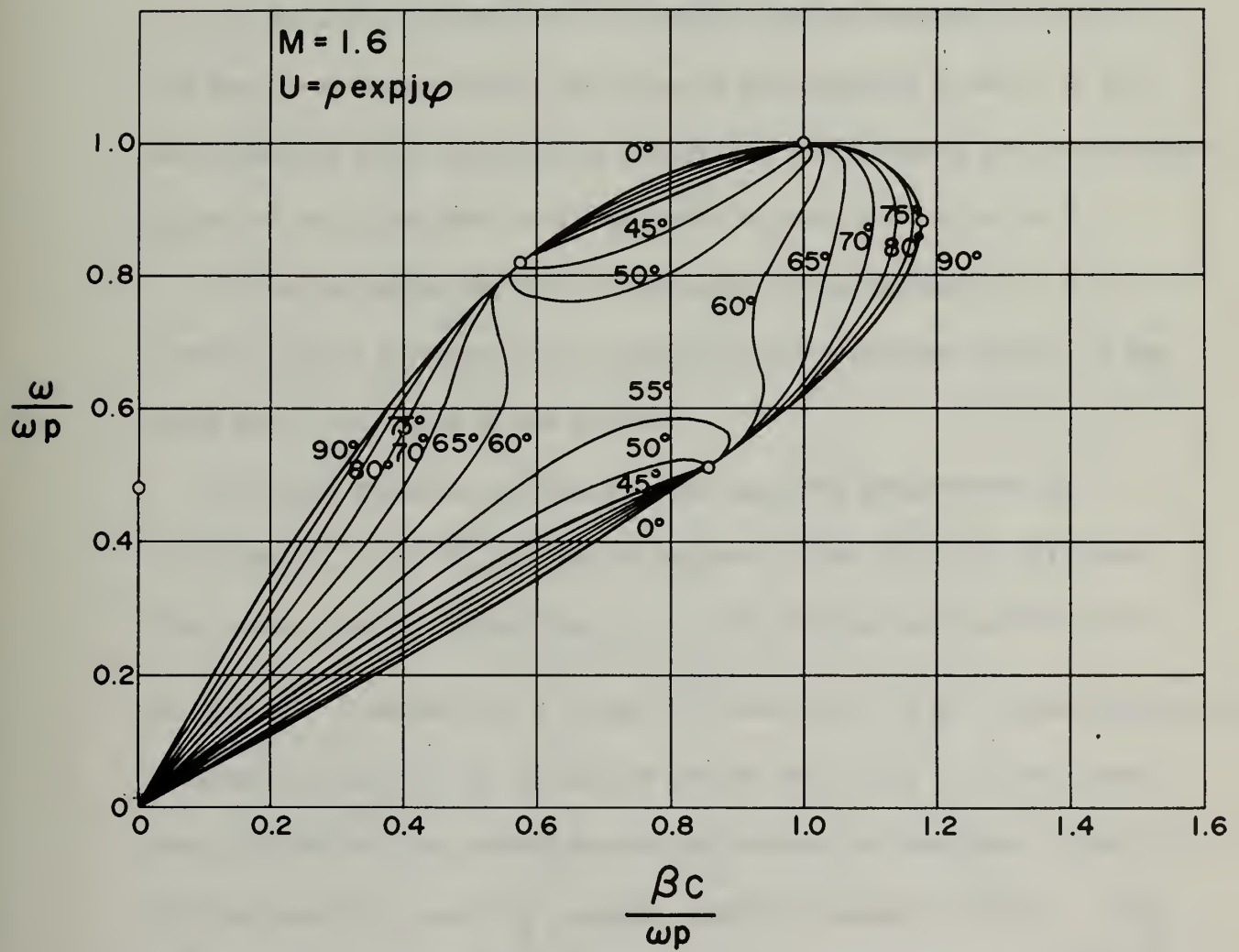


Fig. 9 Contour curves for constant values of the argument  $\varphi$  of the function  $U = \rho \angle \varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .



It is interesting to note the curves delineating various zones in the complex region. On the left boundary of the complex region between the origin and the upper tangent point the value of the argument of  $U$  is  $\pi/2$ , in the upper tangent point the value of the argument is not defined and can assume any value, and between the upper tangent point and the point  $(X=1, Y=1)$  the value of the argument is zero. In this point, again, the argument is not defined.

On the right boundary of the complex region between the origin and the lower tangent point the value of the argument is zero, in the lower tangent point its value is not defined and between the lower tangent point and the point  $(X=1, Y=1)$  the value of the argument is  $\pi/2$ .

On curves where  $\text{Re}(U^2) = 0$  the value of the argument is  $\pi/4$ . Contour curves converge in the upper and lower tangent points, in the point  $(X=1, Y=1)$ , and in the origin.

It is now possible to obtain a picture of the behavior of the functions  $U_1^2$  and  $U_2^2$  in various regions of the  $Y-X$  ( $\omega - \beta$ ) plane. The curves given by Equations 14, 15, 25, 26 and the lines  $Y=1$  and  $Y = \sqrt{1+M^2}$  divide the  $Y-X$  ( $\omega - \beta$ ) plane into 12 or 13 zones depending whether the value of  $M$  is less or greater than unity. It has already been pointed out that within the region defined by Equations 14 and 15 the functions  $U_1^2$  and  $U_2^2$  assume complex conjugate values. In the other regions the following has been found concerning the sign of  $U_1^2$  and  $U_2^2$ :





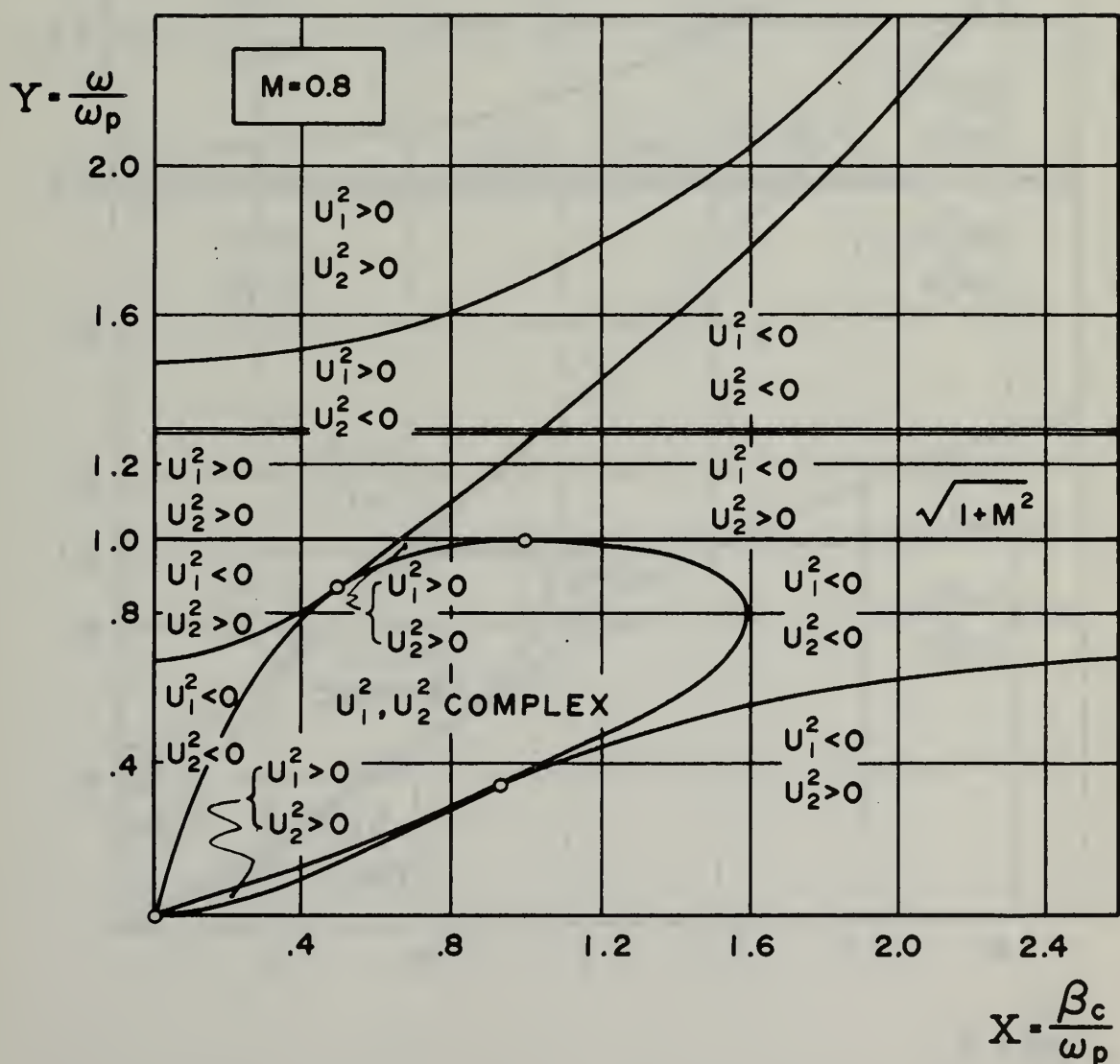


Fig. 10 Zones in the  $\omega - \beta$  plane in which the functions  $U_1^2$  and  $U_2^2$  are of the same or of opposite sign. General behavior for values of  $M < 1$ .





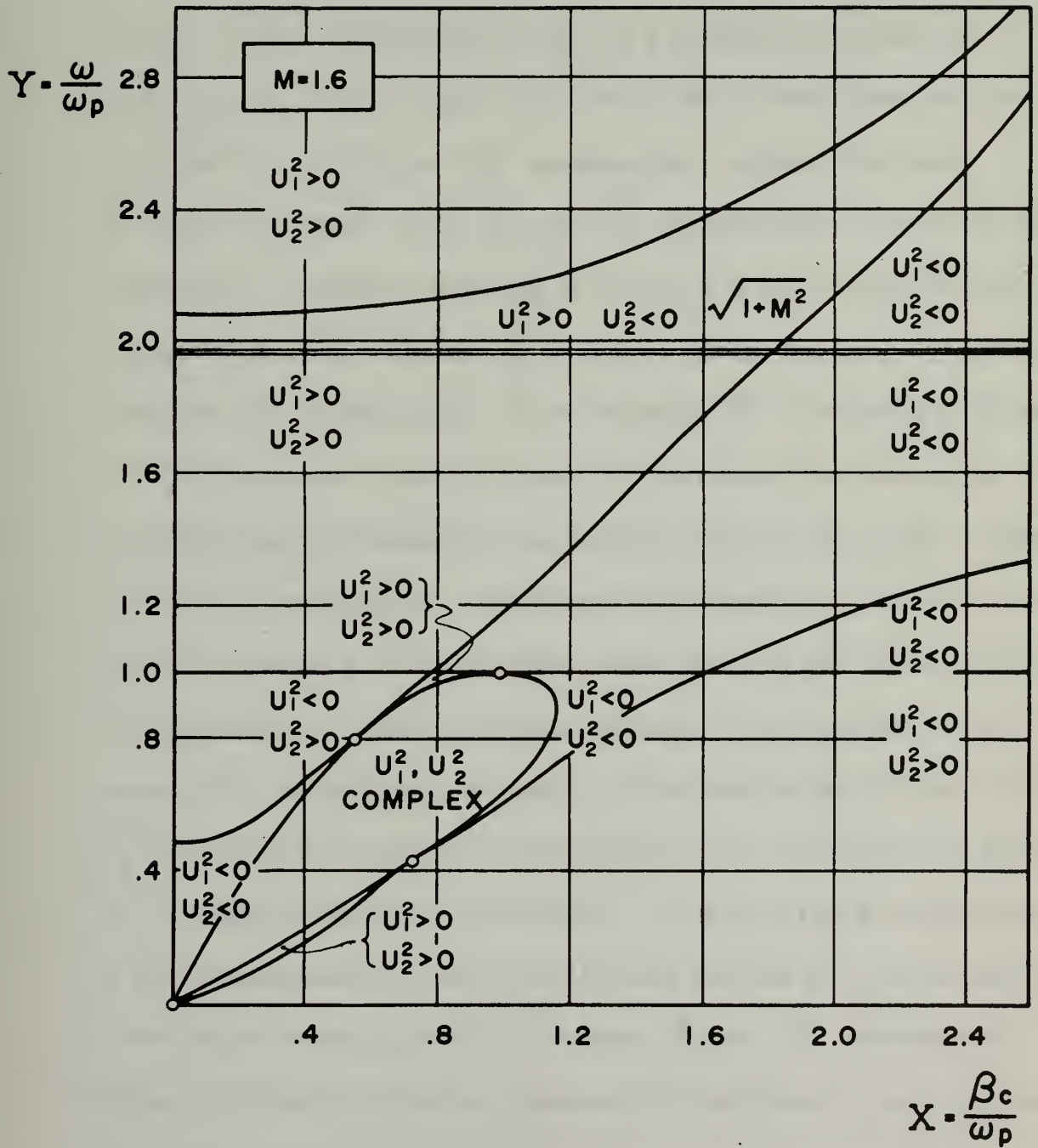


Fig. 11 Zones in the  $\omega$ - $\beta$  plane in which the functions  $U_1^2$  and  $U_2^2$  are of the same or of opposite sign. General behavior for values of  $M > 1$ .



At Values of  $M$  smaller than unity, in the region above the upper branch of the curve given by Eq. 25. Both  $U_1^2$  and  $U_2^2$  are positive. Between the upper branch of the curve given by Eq. 25, and the curve given by Eq. 26, above the straight line  $Y = \sqrt{1+M^2}$ ;  $U_1^2 > 0$ ,  $U_2^2 < 0$ . On the line  $Y = \sqrt{1+M^2}$  the function  $U_2^2$  has a pole while the function  $U_1^2$  is continuous. To the right of the curve of Eq. 26 and above the line  $Y = \sqrt{1+M^2}$  both  $U_1^2$  and  $U_2^2$  are negative. Between the lines  $Y=1$  and  $Y = \sqrt{1+M^2}$  both  $U_1^2$  and  $U_2^2$  are positive to the left of the curve of Eq. 26 while to the right of the curve of Eq. 26 the value of  $U_1^2$  is negative and the value of  $U_2^2$  positive. Under the line  $Y=1$  and above the curve given by Eq. 26 the value of  $U_1^2$  is negative while that of  $U_2^2$  is positive. Under the line  $Y=1$  and under the curve of Eq. 26 and above the left boundary of the complex region given by Eq. 16 both  $U_1^2$  and  $U_2^2$  are positive. Under the curve given by Eq. 26 and to the left of the boundary of this complex region given by Eq. 16 both  $U_1^2$  and  $U_2^2$  are negative. Between the right boundary of the complex region given by Eq. 18 and the lower branch of the curve of Eq. 25 both  $U_1^2$  and  $U_2^2$  are positive. Under the lower branch of the curve of Eq. 25 the function  $U_1^2$  is negative while  $U_2^2$  is positive. To the right of the right boundary of the complex region given by Eq. 18 under the line  $Y=1$  and above the lower branch of the curve of Eq. 25 both  $U_1^2$  and  $U_2^2$  are negative. Figure 10 shows the zones and signs of the functions  $U_1^2$  and  $U_2^2$  for the case when  $M < 1$ .



For values of  $M$  greater than unity the lower branch of the curve given by Eq. 25 and the line  $Y=1$  intersect and modify the picture with the addition of another zone. In such cases the behavior of functions  $U_1^2$  and  $U_2^2$  is modified as follows. To the right of the lower branch of the curve of Eq. 25 and below the line  $Y=1$  the function  $U_1^2$  is negative while  $U_2^2$  is positive. In the newly formed triangular zone bounded by the right boundary of the complex region given by Eq. 18, the line  $Y=1$ , and the lower branch of the curve given by Eq. 25 both  $U_1^2$  and  $U_2^2$  are negative, likewise they are negative in the region above the line  $Y=1$  and below the lower branch of the curve given by Eq. 25. In the region to the right of the curve of Eq. 26, above the line  $Y=1$  and above the lower branch of the curve of Eq. 25 and below the line  $Y=\sqrt{M^2+1}$  the function  $U_1^2$  is negative while the function  $U_2^2$  is positive. The behavior of  $U_1^2$  and  $U_2^2$  in the other zones remains the same as for cases when  $M < 1$ . Figure 11 shows the zones and signs of functions  $U_1^2$  and  $U_2^2$  for this case ( $M > 1$ ).

The partition of the  $\omega - \beta$  ( $Y-X$ ) plane into zones as described above is quite general and is valid for all possible cases. These cases fall under one of the two types, viz., those with  $M < 1$  and those with  $M > 1$ . There is, however, some variation in the sequence of special frequencies ( $Y_2, Y_3, -\frac{M}{2} + \sqrt{\frac{M^2}{4} + 1}, \sqrt{M^2 + 1}$ , etc.) depending in which interval lies the value of  $M$ . The sequential order of these





special frequencies depend only on the values of  $M$ . The possible cases are listed below.

$$0 < M < \frac{1}{\sqrt{2}} \quad (71)$$

$$0 < Y_2 < M < -\frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} < Y_3 < 1 < \sqrt{M^2 + 1} < \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} \quad (72)$$

$$\frac{1}{\sqrt{2}} < M < 1 \quad (73)$$

$$0 < Y_2 < -\frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} < Y_3 < M < 1 < \sqrt{M^2 + 1} < \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} \quad (74)$$

$$1 < M < 1.5 \quad (75)$$

$$0 < Y_2 < -\frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} < Y_3 < 1 < M < \sqrt{M^2 + 1} < \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} \quad (76)$$

$$1.5 < M \quad (77)$$

$$0 < -\frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} < Y_2 < Y_3 < 1 < M < \sqrt{M^2 + 1} < \frac{M}{2} + \sqrt{\frac{M^2}{4} + 1} \quad (78)$$

In addition to the general behavior of the functions  $U_1^2$  and  $U_2^2$  or, if roots are taken,  $U_1$  and  $U_2$ , it is also desirable to have contour representations of these functions in the  $\omega - \beta$  ( $Y-X$ ) plane where  $U_1$





and  $U_2$  have either real or imaginary values, i.e., outside of the complex region.

The equation of contour curves in the  $\omega - \beta$  (Y-X) plane for which U is a real or an imaginary constant can be readily obtained by solving Eq. 3 for X.

$$X^2 = Y^2 - U^2 + \frac{M^2 U^2 + 2Y^2(1-Y^2)}{2(Y^2-1)(Y^2-M^2)} \pm \frac{M \sqrt{4Y^2(Y^2-1)(Y^2-1-U^2) + M^2 U^4}}{2(Y^2-1)(Y^2-M^2)} \quad (79)$$

This is a simple solution of a biquadratic equation in X. For contour curves in the first quadrant of the  $\omega - \beta$  (Y-X) plane only positive values of  $X^2$  are acceptable. There appears to be no simple rule to determine whether the curves obtained from Eq. 79 are the contour curves of  $U_1$  or  $U_2$ . This question can be resolved by calculating with the obtained values of Y and X the desired function  $U_1$  or  $U_2$ , as the case may be, using the rule concerning the selection of the sign as stated above and then determining whether the calculated value is equal to the value of U originally set in Eq. 79. If the calculated value of  $U_1$  or  $U_2$  is equal to the value of U set in Eq. 79 the point in question lies on the curve  $U_1 = \text{constant}$  or  $U_2 = \text{constant}$  respectively.

Equation 3 can also be solved with respect to Y albeit not so readily since the arrangement in powers of Y leads to a biquartic equation.

This biquartic equation can have complex roots and the selection of proper curves is even more laborious in this case. There appears to be no point



in solving the Eq. 3 for  $Y$ , therefore, since the solution with respect to  $X$  can be obtained by simple algebra.

Some representative contour curves for various real and imaginary values of  $U_1$  and  $U_2$  are shown on Figures 12, 13, 14, and 15.



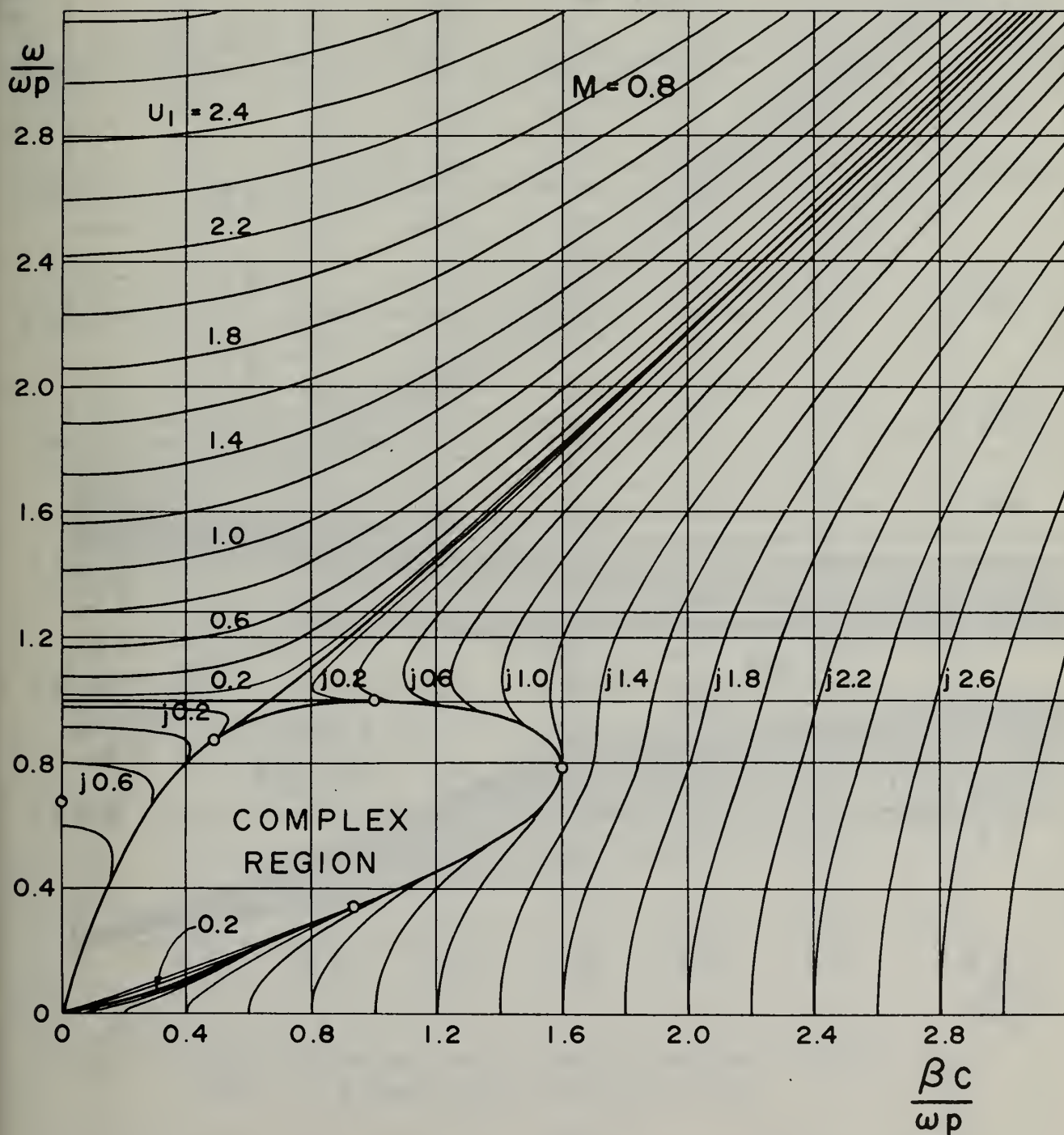


Fig. 12 Contour curves for constant real and imaginary values of  $U_1$  in the  $\omega - \beta$  plane at the value of  $M = 0.8$ .





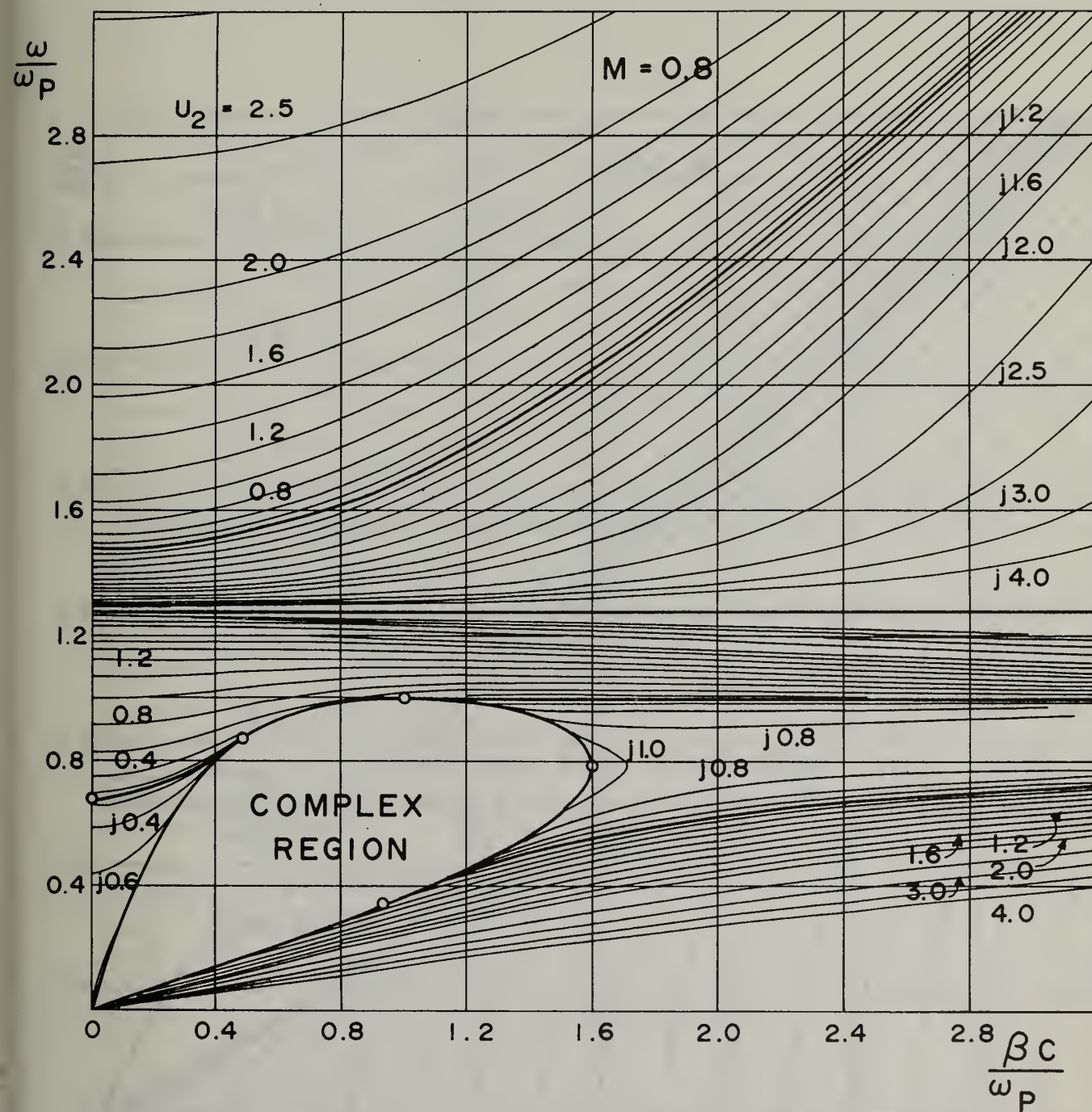


Fig. 13 Contour curves for constant real and imaginary values of  $U_2$  in the  $\omega = \beta$  plane at the value of  $M = 0.8$ .





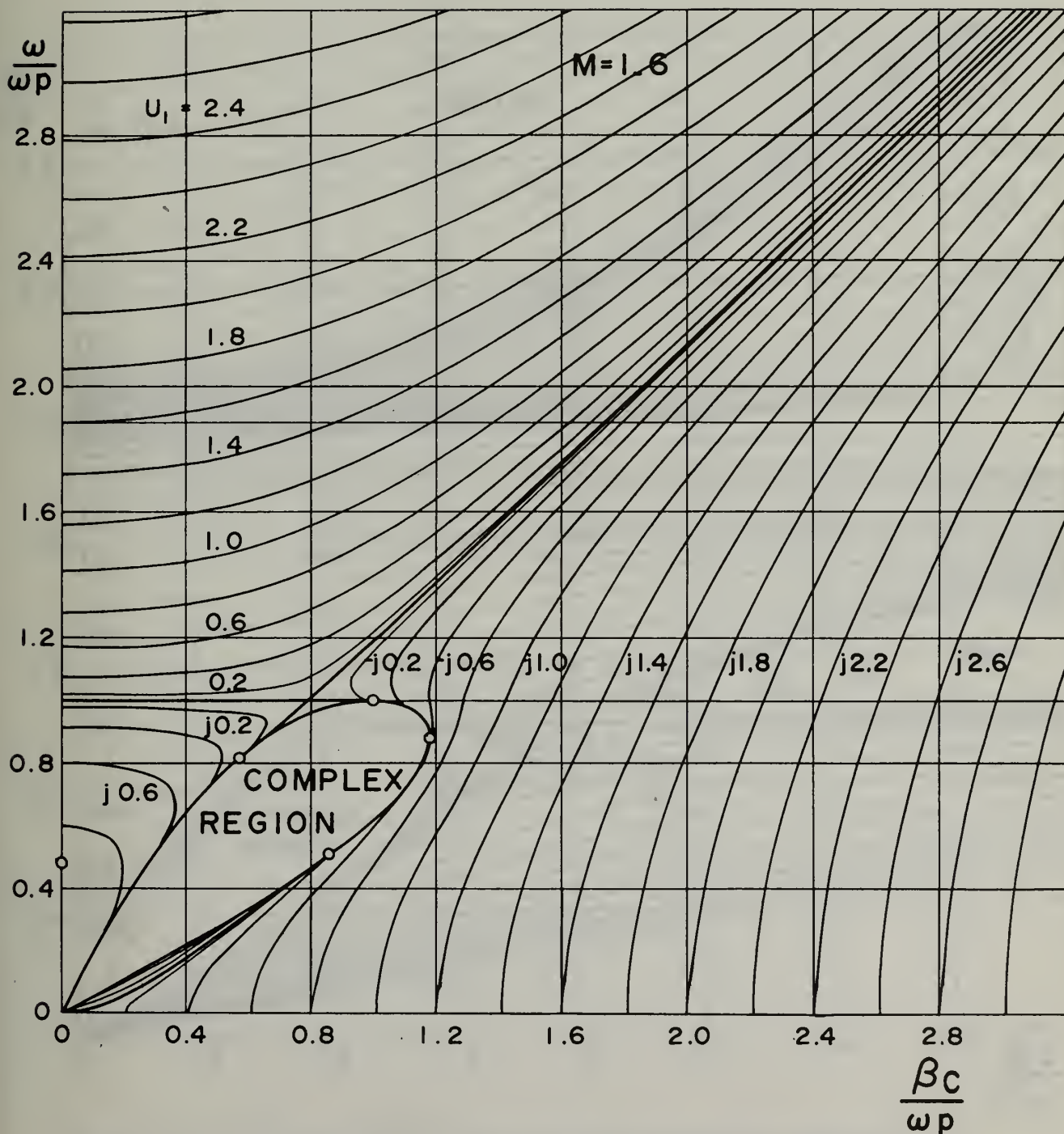


Fig. 14 Contour curves for constant real and imaginary values of  $U_1$  in the  $\omega - \beta$  plane at the value of  $M = 1.6$ .



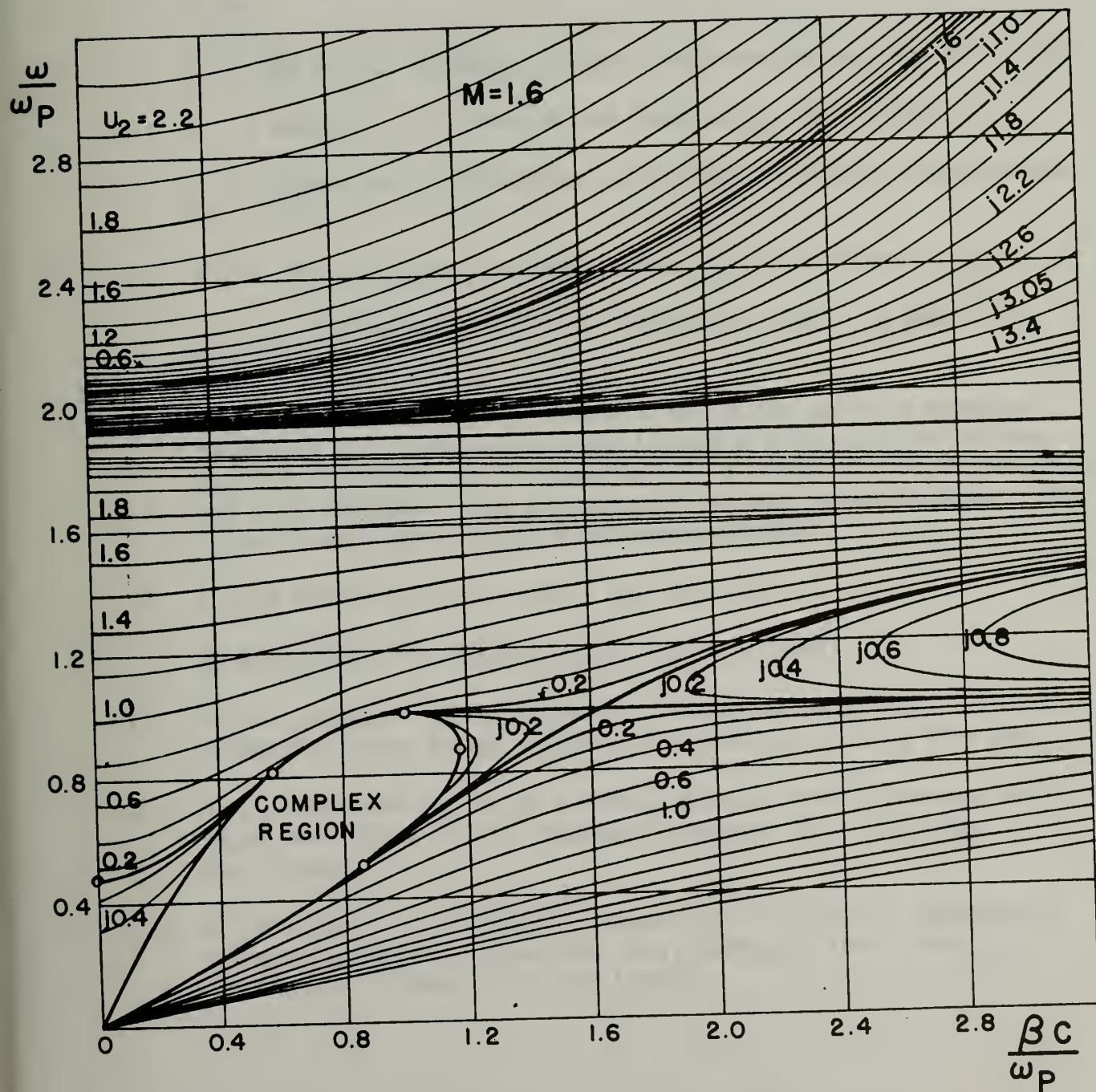


Fig. 15 Contour curves for constant real and imaginary values of  $U_2$  in the  $\omega - \beta$  plane at the value of  $M = 1.6$ .





## REFERENCES

1. A recent paper by H. UNZ, Ohio State University Research Foundation, Report No. 1021-22, Columbus, Ohio, 1962, quotes over 300 articles on related topics.
2. A. W. TRIVELPIECE and R. W. GOULD, J. Appl. Phys, 30, 1784, (1953).
3. S. S. JHA and G. S. KINO, J. Electronics and Control, 14, 167, (1963).
4. G. H. BRYANT, J. Electronics and Control, 12, 297, (1962).
5. R. L. FERRARI and A. REDDISH, Nachrichtentechnische Fachberichte, 22, (1961)
6. W. C. HAHN, General Electric Review, 42, 258, (1939).
7. P. J. B. CLARRICOATS and D. E. CHAMBERS, Proc. IEE (Brit.) 110, 2163, (1963).
8. Properties and definitions of Biradial Functions useful in boundary conditions are discussed in general terms in a memorandum written by C. K. BIRDSALL, G. M. BRANCH, G. S. KINO, G. W. C. MATHERS, and J. C. MIHRAN. This memorandum has been made available to the author through the courtesy of Professor BIRDSALL.
9. A. VAN TRIER, Appl. Sci. Res., B3, 305 (1954).
10. H. SUHL and L. R. WALKER, BSTJ, 33, 579 (1954).
11. See for instance: N. MARCUWITZ, Waveguide Handbook, Vol. 10 of MIT Rad. Lab. Series, McGraw-Hill Book Co., Inc., New York, 1951.
12. See for instance: R. G. E. HUTTER, Beam and Valve Electronics in Microwave Tubes, D. Van Nostrand Company, Inc., Princeton, New Jersey.
13. V. BEVC and T. E. EVERHART, University of California, Electronics Research Laboratory, Report No. 362, Berkeley, 1961 also: J. Electronics & Control, 13, 185 (1962).





14. M. CAMUS and J. LE MEZEC, Centre National D'Études Des Telecommunications, Issy-Les-Mollineaux, Étude No. 674 P.D.T., October 1962. Also: Electromagnetic Theory and Antennas, Proceedings of a Symposium, Copenhagen, June 1962, Macmillan, New York, 1963, Part I, pp. 323-347.
15. B. A. AULD and J. C. EIDSON, J. Appl. Phys., Vol. 34, No. 3, 478-481, (1963).
16. See for instance: Table of Bessel Functions for Complex Arguments, Mathematical Tables Project, L. J. Briggs, Director, Columbia University Press, New York, 1943.



# LIST OF FIGURE CAPTIONS

- Fig. 1 Contour curves for constant values of  $\text{Re}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .
- Fig. 2 Contour curves for constant values of  $\text{Im}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .
- Fig. 3 Contour curves for constant values of  $\text{Re}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .
- Fig. 4 Contour curves for constant values of  $\text{Im}(U^2)$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .
- Fig. 5 Plot of the parameter  $M$  as a function of  $Y(\omega/\omega_p)$  illustrating the solutions of the cubic of Eq. 28.
- Fig. 6 Contour curves for constant values of the modulus  $\rho$  of the function  $U = \rho \angle \varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .
- Fig. 7 Contour curves for constant values of the argument  $\varphi$  of the function  $U = \rho \angle \varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 0.8$ .
- Fig. 8 Contour curves for constant values of the modulus  $\rho$  of the function  $U = \rho \angle \varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .
- Fig. 9 Contour curves for constant values of the argument  $\varphi$  of the function  $U = \rho \angle \varphi$  in the complex region of the  $\omega - \beta$  plane at the value of  $M = 1.6$ .
- Fig. 10 Zones in the  $\omega - \beta$  plane in which the functions  $U_1^2$  and  $U_2^2$  are of the same or of opposite sign. General behavior for values of  $M < 1$ .
- Fig. 11 Zones in the  $\omega - \beta$  plane in which the functions  $U_1^2$  and  $U_2^2$  are of the same or of opposite sign. General behavior for values of  $M > 1$ .
- Fig. 12 Contour curves for constant real and imaginary values of  $U_1$  in the  $\omega - \beta$  plane at the value of  $M = 0.8$ .



- Fig. 13      Contour curves for constant real and imaginary values of  $U_2$   
in the  $\omega - \beta$  plane at the value of  $M = 0.8$ .
- Fig. 14      Contour curves for constant real and imaginary values of  $U_1$   
in the  $\omega - \beta$  plane at the value of  $M = 1.6$ .
- Fig. 15      Contour curves for constant real and imaginary values of  $U_2$   
in the  $\omega - \beta$  plane at the value of  $M = 1.6$ .



LIBRARY DISTRIBUTION LIST  
FOR  
TECHNICAL REPORTS/RESEARCH PAPERS

Documents Department  
General Library  
University of California  
Berkeley 4, California

Librarian  
Lockheed Aircraft Corp.  
California Division  
Dept. 72-25, Bldg. 63-1, Plant A-1  
Burbank, California

Naval Ordnance Test Station  
China Lake California  
Attn: Technical Library

Douglas Aircraft Company, Inc.  
Engineering Library  
El Segundo Division  
827 Lapham Street  
El Segundo, California

Library  
Scripps Institution of Oceanography  
University of California  
La Jolla, California

Librarian  
Government Publications Room  
University of California  
Los Angeles 24, California

Librarian  
Numerical Analysis Research  
University of California  
405 Hilgard Avenue  
Los Angeles 24, California

Librarian  
California Institute of Technology  
Pasadena, California

Mrs. Hilda R. Elledge, Librarian  
Office of Naval Research Branch Office  
1030 East Green Street  
Pasadena 1, California

CONVAIR (San Diego)  
Div. of General Dynamics Corp.  
San Diego 12, California  
Attn: Engineering Library

Librarian  
Ryan Aeronautical Corp.  
Lindbergh Field  
San Diego, California

Commanding Officer and Director  
U. S. Navy Electronic Lab. (Library)  
San Diego 52, California

Mr. Klaus G. Liebhold, Librarian  
TEMPO, General Electric Co.  
725 State Street  
Santa Barbara, California

Document Library  
Stanford University  
Stanford, California

Government Document Division  
University of Colorado Libraries  
Boulder, Colorado

Librarian  
Hamilton Standard Propellers  
East Hartford, Connecticut

The Library  
United Aircraft Corporation  
400 Main Street  
East Hartford 8, Connecticut





LIBRARY DISTRIBUTION LIST FOR TECHNICAL REPORTS/RESEARCH PAPERS (contd.)

Documents Division  
Yale University Library  
New Haven, Connecticut

Librarian  
University of Chicago  
Chicago, Illinois

Librarian  
Bureau of Naval Weapons  
Department of the Navy  
Washington, D. C. 20360

Documents Department  
Northwestern University Library  
Evanston, Illinois

Librarian  
Catholic University of America Library  
Washington 17, D. C.

The Technological Institute, Library  
Northwestern University  
Evanston, Illinois

Librarian  
George Washington University  
Washington 6, D. C.

Librarian  
Purdue University  
Lafayette, Indiana

Librarian  
National Aeronautics and Space Agency  
1512 H Street, N. W.  
Washington, D. C.

Collins Radio Company  
Cedar Rapids, Iowa  
Attn: E. E. Ellison, Librarian

National Bureau of Standards Library  
Room 301, Northwest Building  
Washington 25, D. C.

Librarian  
Glenn L. Martin Company  
Baltimore, Maryland

The Director  
Naval Research Laboratory  
Washington 25, D. C.  
Attn: Code 2021

Librarian  
Johns Hopkins University  
Baltimore, Maryland

Librarian  
U. S. Navy Intelligence School  
U. S. Naval Receiving Station  
Washington 25, D. C.

Documents Office  
University of Maryland Library  
College Park, Maryland

Librarian  
Illinois Institute of Technology  
Chicago 16, Illinois

Librarian  
Applied Physics Laboratory  
Johns Hopkins University  
Silver Spring, Maryland

Commander, U. S. Naval Ordnance Lab.  
White Oak, Silver Spring  
Maryland  
Attn: Library



LIBRARY DISTRIBUTION LIST FOR TECHNICAL REPORTS/RESEARCH PAPERS (contd.)

Librarian  
Technical Library, Code 263a  
Building 39/3  
Boston Naval Shipyard  
Boston 29, Massachusetts

Technical Report Collection  
303A, Pierce Hall  
Harvard University  
Cambridge 38, Massachusetts  
Attn: Mrs. M. L. Cox, Librarian

Massachusetts Institute of Technology  
Serials and Documents  
Hayden Library  
Cambridge 39, Massachusetts

Librarian  
Lowell Technological Institute  
Lowell, Massachusetts

Librarian  
University of Michigan  
Ann Arbor, Michigan

Librarian  
University of Minnesota  
Minneapolis 14, Minnesota

Engineering Library  
Washington University  
St. Louis 5, Missouri

Librarian  
Forrestal Research Center  
Princeton University  
Princeton, New Jersey

Librarian  
Fordham University  
Bronx 58, New York

Librarian  
Cornell Aeronautical Laboratory  
4455 Genesee Street  
Buffalo 21, New York

Library  
Documents Section  
Cornell University  
Ithaca, New York

Librarian  
Grumman Aircraft Engineering Corp.  
Bethpage  
Long Island, New York

Mr. Edward Muhs, Library Supervisor  
Airborne Instruments Laboratory, Inc.  
Walt Whitman Road  
Melville, Long Island, New York

Central Order Records  
Technical Information Library  
Bell Telephone Laboratories  
463 West Street  
New York 17, New York

Columbia University Libraries  
Documents Division  
535 West 114th Street  
New York 27, New York

Librarian  
New York Naval Shipyard  
Material Testing Laboratory  
New York, New York

Scientific Liaison Officer  
Office of Naval Research  
Branch Office, London  
Navy 100, Box 39  
c/o Fleet Post Office  
New York, New York (25 copies)



LIBRARY DISTRIBUTION LIST FOR TECHNICAL REPORTS/RESEARCH PAPERS (contd.)

Engineering Societies Library  
United Engineering Trustees, Inc.  
29 West 39th Street  
New York 18, New York

Librarian  
Special Devices Center  
Port Washington, New York

Librarian  
Rensselaer Polytechnic Institute  
Troy, New York

Librarian  
Documents Division  
Duke University  
Durham, North Carolina

Gift and Exchange Division  
Main Library  
Ohio State University  
Columbus 10, Ohio

Librarian  
University of Oklahoma  
Norman, Oklahoma

Librarian  
Westinghouse Electric Corporation  
Essington, Pennsylvania

Commander  
Philadelphia Naval Shipyard  
Philadelphia 12, Pennsylvania  
Attn: Librarian, Code 263

Librarian  
University of Pennsylvania  
Philadelphia, Pennsylvania

Librarian  
Carnegie Institute of Technology  
Pittsburgh, Pennsylvania

Librarian  
Brown University  
Providence, Rhode Island

Central Research Library  
Oak Ridge National Laboratory  
Post Office Box P  
Oak Ridge, Tennessee

Order Librarian  
Library  
A & M College of Texas  
College Station, Texas

Librarian  
Chance Vought Aircraft, Inc.  
P. O. Box 5907  
Dallas, Texas

Armed Services Technical  
Information Agency  
Arlington Hall Station  
Arlington 12, Virginia (10 copies)

FOREIGN COUNTRIES

Mr. F. W. Gravell, Librarian  
The Patent Office Library  
25, Southampton Buildings  
London, W. C. 2, England

Mr. H. T. Pledge, Keeper of the Library  
The Science Library  
Science Museum  
South Kensington  
London, S. W. 7, England







LIBRARY DISTRIBUTION LIST.FOR TECHNICAL REPORTS/RESEARCH PAPERS (contd.)

Librarian  
National Inst. of Oceanography  
Wormley, Godalming  
Surrey, England

Accession Department  
National Lending Library  
for Science and Technology  
Boston Spa  
Yorkshire, England

Dr. E. Hemlin, Director  
Library  
Chalmers Univ. of Tech.  
Storgatan 43  
Gothenburg C, Sweden



Professor Alan J. Lichtenberg Department of Electrical Engineering University of California Berkeley 4, California	1 Copy
Professor Charles Süsskind Department of Electrical Engineering University of California Berkeley 4, California	1 Copy
Professor Alvin W. Trivelpiece Department of Electrical Engineering University of California Berkeley 4, California	1 Copy
Professor B. J. Clarricoats Department of Electrical Engineering University of Leeds Leeds England	1 Copy
Electronics Research Laboratory University of California Berkeley 4, California	1 Copy
Professor R. N. Carlile Department of Electrical Engineering University of Arizona Tucson, Arizona	1 Copy
Professor S. P. Schlesinger Department of Electrical Engineering Columbia University New York, New York	1 Copy
Microwave Laboratory W. W. Hansen Laboratories of Physics Stanford University Stanford, California	1 Copy
Dr. J. W. Johnston RCA Victor Company, Ltd. Research Laboratories Montreal, Canada	1 Copy
Dr. J. LeMezec Ingenieur Des Télécommunications Au Department "P.D.T." Centre National D'Études Des Télécommunications Issy-Les-Moulineaux France	1 Copy



Professor C. C. Johnson  
University of Utah  
Salt Lake City, Utah

1 Copy

Professor B. Agdur  
Microwave Department  
Royal Institute of Technology  
Stockholm  
Sweden

1 Copy

Dr. R. L. Ferrari  
Research Laboratories of  
The General Electric Company Ltd.  
Wembley  
England

1 Copy

Dr. Vladislav Bevc  
U. S. Naval Postgraduate School  
Monterey, California  
(Code 52 Bv)

10 Copies





## DOCUMENT CONTROL DATA - R&amp;D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) U. S. Naval Postgraduate School Monterey, California 93940		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE Behavior of Gyrotropic Plasma Separation Constants as Functions in the $\omega - \beta$ Plane			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
5. AUTHOR(S) (Last name, first name, initial)  Bevc, Vladislav			
6. REPORT DATE February 1965		7a. TOTAL NO. OF PAGES 54	7b. NO. OF REFS 16
8a. CONTRACT OR GRANT NO.		9a. ORIGINATOR'S REPORT NUMBER(S) Research Paper No. 47	
b. PROJECT NO.			
c.		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d.			
10. AVAILABILITY/LIMITATION NOTICES  Qualified requesters may obtain copies of this report from DDC.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Office of Naval Research	
13. ABSTRACT  The type of the functions appearing in the expression for electromagnetic fields in finite magnetoplasmas depends only on the properties of the medium manifested in the separation constants. The $\omega - \beta$ plane of the Brillouin diagram is partitioned into a definite number of zones characterized by the type of field solutions. The general quantitative behavior of the separation constant for finite magnetoplasma in a longitudinal magnetic field on the Brillouin diagram is described.			



## Security Classification

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Electronic Waveguides Wave Propagation in Electronic Waveguides Bounded Gyrotropic Plasmas Birefringent Media						

## INSTRUCTIONS

1. **ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. **REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. **GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. **REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parentheses immediately following the title.

4. **DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. **AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. **REPORT DATE:** Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

7a. **TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. **NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

8a. **CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. **PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. **ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. **OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (either by the originator or by the sponsor), also enter this number(s).

10. **AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through \_\_\_\_\_."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through \_\_\_\_\_."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through \_\_\_\_\_."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. **SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

12. **SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (paying for) the research and development. Include address.

13. **ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (O), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. **KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, roles, and weights is optional.





1 JUN 65

DISPLAY

TA7

.U6

no.47

Bevc

Behavior of gyrotropic  
plasma separation con-  
stants as functions in  
the W-B plane.

78085

1 JUN 65

DISPLAY

TA7

.U6

no.47

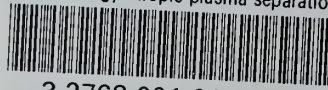
Bevc

Behavior of gyrotropic  
plasma separation con-  
stants as functions in  
the W-B plane.

78085

genTA 7.U6 no.47

Behavior of gyrotropic plasma separation



3 2768 001 61490 2

DUDLEY KNOX LIBRARY